



Tanta
University

Electrical Power and Machines Engineering
Electromagnetic Fields: Sheet 1



Faculty of
Engineering

- Given the vectors $\vec{M} = -10\vec{a}_x + 4\vec{a}_y - 8\vec{a}_z$ and $\vec{N} = 8\vec{a}_x + 7\vec{a}_y - 2\vec{a}_z$, find (a) a unit vector in the direction of $-\vec{M} + 2\vec{N}$; (b) the magnitude of $5\vec{a}_x + \vec{N} - 3\vec{M}$ and (c) the value of $|\vec{M}||2\vec{N}|(\vec{M} + \vec{N})$.
- Vector \vec{A} extends from the origin to point (1, 2, 3), and vector \vec{B} extends from the origin to (2, 3, -2). Find (a) the unit vector in the direction of $(\vec{A} - \vec{B})$; (b) the unit vector in the direction of the line extending from the origin to the midpoint of the line joining the ends of \vec{A} and \vec{B} .
- The vector from the origin to point A is given as (6, -2, -4), and the unit vector directed from the origin toward point B is (2, -2, 1)/3. If points A and B are ten units apart, find the coordinates of point B.
- Find the acute angle between the two vectors $\vec{A} = 2\vec{a}_x + \vec{a}_y + 3\vec{a}_z$ and $\vec{B} = \vec{a}_x - 3\vec{a}_y + 2\vec{a}_z$ by using the definition of (a) the dot product and (b) the cross product.
- Given the points $M(0.1, -0.2, -0.1)$, $N(-0.2, 0.1, 0.3)$, and $P(0.4, 0, 0.1)$, find (a) the vector \vec{R}_{MN} ; (b) the dot product $\vec{R}_{MN} \cdot \vec{R}_{MP}$; (c) the scalar projection of \vec{R}_{MN} on \vec{R}_{MP} ; (d) the angle between \vec{R}_{MN} and \vec{R}_{MP} .
- Find (a) the vector component of $\vec{F} = 10\vec{a}_x - 6\vec{a}_y + 5\vec{a}_z$ that is parallel to $\vec{G} = 0.1\vec{a}_x + 0.2\vec{a}_y + 0.3\vec{a}_z$; (b) the vector component of \vec{F} that is perpendicular to \vec{G} ; (c) the vector component of \vec{G} that is perpendicular to \vec{F} .
- Three vectors extending from the origin are given as $\vec{R}_1 = (7, 3, -2)$, $\vec{R}_2 = (-2, 7, -3)$, and $\vec{R}_3 = (0, 2, 3)$. Find (a) a unit vector perpendicular to both \vec{R}_1 and \vec{R}_2 ; (b) a unit vector perpendicular to the vectors $\vec{R}_1 - \vec{R}_2$ and $\vec{R}_2 - \vec{R}_3$; (c) the area of the triangle defined by \vec{R}_1 and \vec{R}_2 ; (d) the area of the triangle defined by the heads of \vec{R}_1 , \vec{R}_2 , and \vec{R}_3 .
- Express in cylindrical components: (a) the vector from $C(3, 2, -7)$ to $D(-1, -4, 2)$; (b) a unit vector at D directed toward C; (c) a unit vector at D directed toward the origin.
- The surfaces $r = 2$ and 4 , $\theta = 30^\circ$ and 50° , and $\phi = 20^\circ$ and 60° identify a closed surface. Find (a) the enclosed volume; (b) the total area of the enclosing surface; (c) the total length of the twelve edges of the surface; (d) the length of the longest straight line that lies entirely within the surface.
- Express the unit vector \hat{a}_x in spherical components at the point: (a) $r = 2\text{m}$, $\theta = 1\text{rad}$, $\phi = 0.8\text{rad}$; (b) $x = 3\text{m}$, $y = 2\text{m}$, $z = -1\text{m}$; (c) $\rho = 2.5\text{m}$, $\phi = 0.7\text{rad}$, $z = 1.5\text{m}$.

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1. Given the vectors $M = -10a_x + 4a_y - 8a_z$ and $N = 8a_x + 7a_y - 2a_z$, FIND :

(a) a unit vector in the direction of $-M + 2N$;

(b) the magnitude of $5a_x + N - 3M$

(c) the value of $|M||2N|(M + N)$.

a)

$$\begin{aligned} -M + 2N &= -(-10a_x + 4a_y - 8a_z) + 2(8a_x + 7a_y - 2a_z) \\ &= (10a_x - 4a_y + 8a_z) + (16a_x + 14a_y - 4a_z) = 26a_x + 10a_y + 4a_z \end{aligned}$$

$$|-M + 2N| = \sqrt{26^2 + 10^2 + 4^2} = 6\sqrt{22}$$

$$\text{unit vector} = \frac{26a_x + 10a_y + 4a_z}{6\sqrt{22}} = 0.9238a_x + 0.355334a_y + 0.142133a_z$$

b)

$$5a_x + N - 3M = 5a_x + (8a_x + 7a_y + 2a_z) - 3(-10a_x + 4a_y - 8a_z)$$

$$= 43a_x - 5a_y - 6a_z$$

$$|5a_x + N - 3M| = \sqrt{43^2 + 5^2 + 6^2} = 43.7035$$

c)

$$|M| = \sqrt{10^2 + 4^2 + 8^2} = 6\sqrt{5} = 13.4164$$

$$|2N| = \sqrt{16^2 + 14^2 - 4^2} = 2\sqrt{109} = 20.88061$$

$$\bar{M} + \bar{N} = (-10a_x + 4a_y - 8a_z) + (8a_x + 7a_y + 2a_z) = -2a_x + 11a_y - 6a_z$$

$$\therefore |M||2N|(\bar{M} + \bar{N}) = (13.416)(20.88)(-2a_x + 11a_y - 6a_z) = -560.25a_x + 3081.38a_y - 1680.75a_z$$

2. Vector A extends from the origin to point (1, 2, 3), and vector B extends from the origin to (2, 3, -2). Find

(a) the unit vector in the direction of $(A-B)$;

(b) the unit vector in the direction of the line extending from the origin to the midpoint of the line joining the ends of A and B.

a)

$$\bar{A} = 1a_x + 2a_y + 3a_z$$

$$\bar{B} = 2a_x + 3a_y - 2a_z$$

$$\bar{A} - \bar{B} = (1a_x + 2a_y + 3a_z) - (2a_x + 3a_y - 2a_z)$$

$$= -1a_x - 1a_y + 1a_z$$

$$|\bar{A} - \bar{B}| = \sqrt{1^2 + 1^2 + 1^2} = \sqrt{3}$$

$$\text{unit vector} = \frac{-1a_x - 1a_y + 1a_z}{\sqrt{3}} = -\frac{1}{\sqrt{3}}a_x - \frac{1}{\sqrt{3}}a_y + \frac{1}{\sqrt{3}}a_z$$

b)

$$\text{the midpoint} = \frac{1+2}{2} a_x + \frac{2+3}{2} a_y + \frac{3+2}{2} a_z = 1.5 a_x + 2.5 a_y + 2.5 a_z$$

$$\text{it's magnitude} = \sqrt{1.5^2 + 2.5^2 + 2.5^2} = 3.34057$$

$$\text{unit vector} = \frac{1.5 a_x + 2.5 a_y + 2.5 a_z}{3.34057} = 0.3905 a_x + 0.6509 a_y + 0.6509 a_z$$

3. The vector from the origin to point A is given as (6, -2, -4), and the unit vector directed from the origin toward point B is (2, -2, 1)/3. If points A and B are ten units apart, find the coordinates of point B.

$$A = 6 a_x - 2 a_y - 4 a_z$$

$$B \text{ unit vector} = \frac{2}{3} a_x - \frac{2}{3} a_y + \frac{1}{3} a_z$$

$$\therefore B = \frac{2}{3} k a_x - \frac{2}{3} k a_y + \frac{1}{3} k a_z$$

$$\because |\vec{AB}| = |B - A| = 10 \text{ units}$$

$$\sqrt{\left(\frac{2}{3}k - 6\right)^2 + \left(-\frac{2}{3}k + 2\right)^2 + \left(\frac{1}{3}k + 4\right)^2} = 10$$

$$\left(\frac{2}{3}k - 6\right)^2 + \left(-\frac{2}{3}k + 2\right)^2 + \left(\frac{1}{3}k + 4\right)^2 = 100$$

$$\text{put } C = \frac{2}{3}k$$

$$(C - 6)^2 + (-C + 2)^2 + \left(\frac{C}{2} + 4\right)^2 = 100$$

$$C^2 - 12C + 36 + C^2 - 4C + 4 + \frac{C^2}{4} + 4C + 16 = 100$$

$$\left(1 + 1 + \frac{1}{4}\right)C^2 + (-12 - 4 + 4)C + (36 + 4 + 16) = 100$$

$$2.25C^2 - 12C - 44 = 0$$

$$\therefore C = 7.8306 \quad \text{or} \quad -2.497$$

$$\therefore k = \frac{3}{2} C = 11.7459 \quad \text{or} \quad -3.7455$$

$$\therefore B = \frac{2}{3}k a_x - \frac{2}{3}k a_y + \frac{1}{3}k a_z$$

$$\vec{B} = 7.8306 a_x - 7.8306 a_y + 3.9153 a_z$$

or

$$\vec{B} = -2.497 a_x + 2.497 a_y - 1.2458 a_z$$

4. Find the acute angle between the two vectors $A = 2a_x + a_y + 3a_z$ and $B = a_x - 3a_y + 2a_z$ by using the definition of (a) the dot product and (b) the cross product.

a) using the dot product

$$A = \sqrt{2^2 + 1^2 + 3^2} = \sqrt{14} = 3.741$$

$$B = \sqrt{1^2 + 3^2 + 2^2} = \sqrt{14} = 3.741$$

$$\vec{A} \cdot \vec{B} = (2a_x + a_y + 3a_z) \cdot (a_x - 3a_y + 2a_z)$$

$$= 2 - 3 + 6 = 5 = AB \cos(\theta) = 14 \cos(\theta)$$

$$\therefore \cos(\theta) = \frac{5}{14}$$

$$\therefore \theta = \cos^{-1}\left(\frac{5}{14}\right) = 69.07^\circ = 1.2 \text{ rad}$$

b) using the cross product

$$\vec{A} \times \vec{B} = \begin{bmatrix} a_x & a_y & a_z \\ 2 & 1 & 3 \\ 1 & -3 & 2 \end{bmatrix} = (2+9)a_x - (4-3)a_y + (-6-1)a_z = 11a_x - a_y - 7a_z$$

$$\therefore |\vec{A} \times \vec{B}| = \sqrt{11^2 + 1^2 + 7^2} = 3\sqrt{19} = 13.0766 = AB \sin(\theta) = 14 \sin(\theta)$$

$$\therefore \sin(\theta) = \frac{3\sqrt{19}}{14}$$

$$\therefore \theta = \sin^{-1}\left(\frac{3\sqrt{19}}{14}\right) = 69.07^\circ = 1.2 \text{ rad}$$

5. Given the points $M(0.1, -0.2, -0.1)$, $N(-0.2, 0.1, 0.3)$, and $P(0.4, 0, 0.1)$, find

(a) the vector \overrightarrow{RMN} ; (b) the dot product $\overrightarrow{RMN} \cdot \overrightarrow{RMP}$; (c) the scalar projection of \overrightarrow{RMN} on \overrightarrow{RMP} ; (d) the angle between \overrightarrow{RMN} and \overrightarrow{RMP} .

a)

$$\overrightarrow{RMN} = \vec{N} - \vec{M} = -0.3 a_x + 0.3 a_y + 0.4 a_z$$

$$|\overrightarrow{RMN}| = \sqrt{0.3^2 + 0.3^2 + 0.4^2} = 0.583$$

$$\overrightarrow{RMP} = \vec{P} - \vec{M} = 0.3 a_x + 0.2 a_y + 0.2 a_z$$

$$|\overrightarrow{RMP}| = \sqrt{0.3^2 + 0.2^2 + 0.2^2} = 0.41231$$

b)

$$\begin{aligned} \overrightarrow{RMN} \cdot \overrightarrow{RMP} &= (-0.3 a_x + 0.3 a_y + 0.4 a_z) \cdot (0.3 a_x + 0.2 a_y + 0.2 a_z) \\ &= -0.09 + 0.06 + 0.08 = 0.05 \end{aligned}$$

c)

$$\text{the scalar projection} = \frac{\overrightarrow{RMN} \cdot \overrightarrow{RMP}}{|\overrightarrow{RMP}|} = \frac{0.05}{0.41231} = 0.12126$$

d)

$$\overrightarrow{RMN} \cdot \overrightarrow{RMP} = |\overrightarrow{RMN}| |\overrightarrow{RMP}| \cos(\theta) = 0.583 * 0.4123 \cos(\theta) = 0.05$$

$$\therefore \theta = \cos^{-1}\left(\frac{0.05}{0.240}\right) = 77.9^\circ \approx 78^\circ = 1.361 \text{ rad}$$

6. Find (a) the vector component of $F = 10a_x - 6a_y + 5a_z$ that is parallel to $G = 0.1a_x + 0.2a_y + 0.3a_z$; (b) the vector component of F that is perpendicular to G ; (c) the vector component of G that is perpendicular to F .

$$|F| = \sqrt{10^2 + 6^2 + 5^2} = 12.688$$

$$|G| = \sqrt{0.1^2 + 0.2^2 + 0.3^2} = 0.37416$$

a)

$$\begin{aligned} \overline{F \cdot G} &= \frac{F \cdot G}{|G|} = \frac{(1 + (-1.2) + 1.5)}{0.37416} = 3.474 \\ \overline{a_g} &= \frac{0.1a_x + 0.2a_y + 0.3a_z}{0.37416} = 0.2672 a_x + 0.5345 a_y + 0.8018 a_z \\ \therefore F \text{ parallel component to } G &= 3.474 (0.2672 a_x + 0.5345 a_y + 0.8018 a_z) \\ \overline{F_{\parallel}} &= \mathbf{0.928 a_x + 1.85 a_y + 2.78 a_z} \end{aligned}$$

b)

F perpendicular to G

$$\begin{aligned} \overline{F} &= \overline{F_{\parallel}} + \overline{F_{\perp}} \\ \therefore \overline{F_{\perp}} &= \overline{F} - \overline{F_{\parallel}} = (10a_x - 6a_y + 5a_z) - (0.928 a_x + 1.85 a_y + 2.78 a_z) \\ \overline{F_{\perp}} &= \mathbf{9.072 a_x - 7.85 a_y + 2.22 a_z} \end{aligned}$$

c)

G component perpendicular on F

$$\begin{aligned} \overline{G_{\perp}} &= \overline{G} - \overline{G_{\parallel}} \\ &= (0.1a_x + 0.2a_y + 0.3a_z) - \left(\frac{F \cdot G}{|F|} \right) \overline{a_f} \\ &= (0.1a_x + 0.2a_y + 0.3a_z) - \left(\frac{(1 + (-1.2) + 1.5)}{12.688} \right) \overline{a_f} \\ \overline{a_f} &= \frac{(10a_x - 6a_y + 5a_z)}{12.688} = 0.788 a_x - 0.472 a_y + 0.39 a_z \\ \therefore \left(\frac{F \cdot G}{|F|} \right) \overline{a_f} &= 0.102 (0.788 a_x - 0.472 a_y + 0.39 a_z) = 0.080376 a_x - 0.048144 a_y + 0.03978 a_z \\ \therefore \overline{G_{\perp}} &= (0.1a_x + 0.2a_y + 0.3a_z) - (0.080376 a_x - 0.048144 a_y + 0.03978 a_z) \\ \overline{G_{\perp}} &= \mathbf{0.019624 a_x + 0.248144 a_y + 0.26022 a_z} \end{aligned}$$

7. Three vectors extending from the origin are given as $R_1 = (7, 3, -2)$, $R_2 = (-2, 7, -3)$, and $R_3 = (0, 2, 3)$. Find (a) a unit vector perpendicular to both R_1 and R_2 ; (b) a unit vector perpendicular to the vectors $R_1 - R_2$ and $R_2 - R_3$; (c) the area of the triangle defined by R_1 and R_2 ; (d) the area of the triangle defined by the heads of R_1 , R_2 , and R_3 .

a)

$$\begin{aligned} \text{a vector } \bar{n} \text{ is perpendicular on } \overline{R_1} \text{ and } \overline{R_2} \text{ if} \\ \bar{n} = \overline{R_1} \times \overline{R_2} = (7, 3, -2) \times (-2, 7, -3) &= \begin{bmatrix} a_x & a_y & a_z \\ 7 & 3 & -2 \\ -2 & 7 & -3 \end{bmatrix} = 5 a_x + 25 a_y + 55 a_z \end{aligned}$$

$$\therefore \text{ a unit vector } \overline{a_n} = \frac{5 a_x + 25 a_y + 55 a_z}{\sqrt{5^2 + 25^2 + 55^2}} = \left(\frac{\sqrt{(75626)} * a_x + \sqrt{(75626)} * 5 a_y + \sqrt{(75626)} * 11 a_z}{75626} \right) =$$

$$\overline{a_n} = \mathbf{0.00363 a_x + 0.018181 a_y + 0.0399 a_z}$$

b)

$$\overline{R_1} - \overline{R_2} = (7, 3, -2) - (-2, 7, -3) = 9 a_x - 4 a_y + a_z$$

$$\overline{R_2} - \overline{R_3} = (-2, 7, -3) - (0, 2, 3) = -2 a_x + 5 a_y - 6 a_z$$

a vector z will be perpendicular on both of them if

$$z = (\overline{R_1} - \overline{R_2}) \times (\overline{R_2} - \overline{R_3}) = \begin{bmatrix} a_x & a_y & a_z \\ 9 & -4 & 1 \\ -2 & 5 & -6 \end{bmatrix} = 19 a_x + 52 a_y + 37 a_z$$

$$\therefore \overline{a_z} = \frac{19 a_x + 52 a_y + 37 a_z}{\sqrt{19^2 + 52^2 + 37^2}} = \frac{19 a_x + 52 a_y + 37 a_z}{66.588287258346} = \mathbf{0.285 a_x + 0.7809 a_y + 0.556 a_z}$$

c)

$$\text{the area of the triangle} = \frac{1}{2} |\overline{R_1} \times \overline{R_2}|$$

$$\overline{R_1} \times \overline{R_2} = 5 a_x + 25 a_y + 55 a_z \text{ from (a)}$$

$$\therefore \frac{1}{2} |\overline{R_1} \times \overline{R_2}| = \frac{1}{2} * \sqrt{5^2 + 25^2 + 55^2} = \mathbf{30.311 \text{ Square Units}}$$

d)

the two vectors that determine this triangle are $\overline{R_1 R_2}$ and $\overline{R_1 R_3}$

$$\overline{R_1 R_2} = \overline{R_2} - \overline{R_1} = -9 a_x + 4 a_y - 1 a_z$$

$$\overline{R_1 R_3} = \overline{R_3} - \overline{R_1} = -7 a_x - 1 a_y + 5 a_z$$

$$\therefore \text{ the Area} = \frac{1}{2} |\overline{R_1 R_2} \times \overline{R_1 R_3}|$$

$$\overline{R_1 R_2} \times \overline{R_1 R_3} = \begin{bmatrix} a_x & a_y & a_z \\ -9 & 4 & -1 \\ -7 & -1 & 5 \end{bmatrix} = 19 a_x + 52 a_y + 37 a_z$$

$$\therefore = \frac{1}{2} |\overline{R_1 R_2} \times \overline{R_1 R_3}| = \frac{1}{2} \sqrt{19^2 + 52^2 + 37^2} = \mathbf{33.294 \text{ square units}}$$

8. Express in cylindrical components: (a) the vector from $C(3, 2, -7)$ to $D(-1, -4, 2)$; (b) a unit vector at D directed toward C ; (c) a unit vector at D directed toward the origin.

a)

$$\text{The vector } \overline{CD} = \overline{D} - \overline{C} = -4 a_x - 6 a_y + 9 a_z$$

to cylindrical $\overline{CD} * \overline{a_\rho} = -4 a_x \cdot \overline{a_\rho} - 6 a_y \cdot \overline{a_\rho} + 9 a_z \cdot \overline{a_\rho} = -4 \cos(\phi) - 6 \sin(\phi)$
 $\overline{CD} * \overline{a_\phi} = -4 a_x \cdot \overline{a_\phi} - 6 a_y \cdot \overline{a_\phi} + 9 a_z \cdot \overline{a_\phi} = 4 \sin(\phi) - 6 \cos(\phi)$
 $\overline{CD} * \overline{a_z} = -4 a_x \cdot \overline{a_z} - 6 a_y \cdot \overline{a_z} + 9 a_z \cdot \overline{a_z} = 9$
 \therefore in cylindrical $\overline{CD} = (-4 \cos(\phi) - 6 \sin(\phi)) \overline{a_\rho} + (4 \sin(\phi) - 6 \cos(\phi)) \overline{a_\phi} + 9 \overline{a_z}$
where $\phi = \tan^{-1} \left(\frac{y}{x} \right)$, for point (x, y, z)

b) a unit vector \overline{DC}

$$\overline{DC} = \overline{C} - \overline{D} = (3, 2, -7) - (-1, -4, 2) = 4 a_x + 6 a_y - 9 a_z$$

$$\therefore \text{unit vector} = \frac{4 a_x + 6 a_y - 9 a_z}{\sqrt{4^2 + 6^2 + 9^2}} = 0.347 a_x + 0.52 a_y - 0.78 a_z$$

$$\widehat{DC}(\text{unit vector}) * \overline{a_\rho} = 0.347 \cos(\phi) + 0.347 \sin(\phi)$$

$$\widehat{DC}(\text{unit vector}) * \overline{a_\phi} = -0.347 \sin(\phi) + 0.347 \cos(\phi)$$

$$\widehat{DC}(\text{unit vector}) * \overline{a_z} = -0.78$$

$$\therefore \text{in cylindrical } \widehat{DC} = (0.347 \cos(\phi) + 0.347 \sin(\phi)) a_\rho + (-0.347 \sin(\phi) + 0.347 \cos(\phi)) a_\phi - 0.78 a_z$$

where $\phi = \tan^{-1} \left(\frac{y}{x} \right)$

c) $\overline{DO} = (0, 0, 0) - (-1, -4, 2) = 1 a_x + 4 a_y - 2 a_z$

$$\widehat{DO} = \frac{1 a_x + 4 a_y - 2 a_z}{\sqrt{1^2 + 4^2 + 2^2}} = 0.218 a_x + 0.873 a_y - 0.436 a_z$$

to cylindrical :

$$(0.218 \cos(\phi) + 0.873 \sin(\phi)) a_\rho + (-0.218 \sin(\phi) + 0.873 \cos(\phi)) a_\phi - 0.436 a_z$$

9. The surfaces $r = 2$ and 4 , $\theta = 30^\circ$ and 50° , and $\phi = 20^\circ$ and 60° identify a closed surface. Find (a) the enclosed volume; (b) the total area of the enclosing surface; (c) the total length of the twelve edges of the surface; (d) the length of the longest straight line that lies entirely within the surface.



10. Express the unit vector \hat{a}_x in spherical components at the point:

(a) $r = 2\text{m}$, $\theta = 1\text{rad}$, $\phi = 0.8\text{rad}$; (b) $x = 3\text{m}$, $y = 2\text{m}$, $z = -1\text{m}$; (c) $\rho = 2.5\text{m}$, $\phi = 0.7\text{rad}$, $z = 1.5\text{m}$.

	\mathbf{a}_r	\mathbf{a}_θ	\mathbf{a}_ϕ
\mathbf{a}_x	$\sin \theta \cos \phi$	$\cos \theta \cos \phi$	$-\sin \phi$

$$a_x = (\sin \theta \cos \phi) \overline{a_r} + (\cos \theta \cos \phi) \overline{a_\theta} - \sin \phi a_\phi$$

a)

$$\begin{aligned} a_x &= (\sin 1 \cos 0.8) \overline{a_r} + (\cos 1 \cos 0.8) \overline{a_\theta} - \sin 0.8 a_\phi \\ &= (0.5863) \overline{a_r} + (0.3764) \overline{a_\theta} - 0.7174 a_\phi \end{aligned}$$

b)

first we convert the point to spherical coordinates

$$r = \sqrt{x^2 + y^2 + z^2} = \sqrt{3^2 + 2^2 + (-1)^2} = \sqrt{14} = 3.7417$$

$$\theta = \cos^{-1} \left(\frac{z}{r} \right) = \cos^{-1} \left(\frac{-1}{\sqrt{14}} \right) = 105.5014^\circ$$

$$\phi = \tan^{-1} \left(\frac{y}{x} \right) = \tan^{-1} \left(\frac{2}{3} \right) = 33.6901^\circ$$

$$\begin{aligned} \therefore a_x &= (\sin 105.5 \cos 33.69) \overline{a_r} + (\cos 105.5 \cos 33.69) \overline{a_\theta} - \sin 33.69 a_\phi \\ &= (0.8018) \overline{a_r} + (-0.2224) \overline{a_\theta} - 0.5547 a_\phi \end{aligned}$$

c)

convert it to cartesian

$$x = \rho \cos \phi = 2.5 \cos 0.7 = 1.9121 \text{ m}$$

$$y = \rho \sin \phi = 2.5 \sin 0.7 = 1.6105 \text{ m}$$

$$z = 1.5 \text{ m}$$

to spherical

$$r = \sqrt{1.9^2 + 1.6^2 + 1.5^2} = 2.9017$$

$$\theta = \cos^{-1} \left(\frac{1.5}{2.9} \right) = 58.8526^\circ$$

$$\phi = \tan^{-1} \left(\frac{1.6}{1.9} \right) = 40.1009^\circ$$

$$\begin{aligned} a_x &= (\sin 58.8526 \cos 40.1) \overline{a_r} + (\cos 58.8526 \cos 40.1) \overline{a_\theta} - \sin 40.1 a_\phi \\ &= (0.6546) \overline{a_r} + (0.3956) \overline{a_\theta} - 0.6441 a_\phi \end{aligned}$$



1. Find the volume defined by:
 - (a) $3 < r < 5$, $0.1\pi < \theta < 0.3\pi$ and $1.2\pi < \phi < 1.6\pi$
 - (b) $4 < \rho < 6$, $2 < Z < 5$ and $30^\circ < \phi < 60^\circ$
2. Find the area of:
 - (a) Curved surface of right circular cylinder with $\rho = 2$ m, $0 < Z < 5$ and $30^\circ < \phi < 120^\circ$
 - (b) Strip $0 < \theta < \pi$ on a spherical shell of radius r
3. Transfer $\mathbf{G} = \frac{xz}{y} \mathbf{a}_x$ into:
 - (a) Cylindrical coordinates system
 - (b) Spherical coordinates system
4. Using the coordinate system named, give vector at point A (2,1,-3) that extends to B (1,3,4) using: (a) Cartesian (b) Cylindrical (c) Spherical
5. Find the gradient of theses scalar fields:
 - (a) $U = 4xz^2 + 3yz$
 - (b) $W = 2\rho(z^2 + 1) \cos \phi$
 - (c) $H = r^2 \cos \theta \cos \phi$
6. In the region of free space that includes the volume, $2 < x, y, z < 3$,

$$\mathbf{D} = \frac{z}{z^2} (yz \mathbf{a}_x + xz \mathbf{a}_y - 2xz \mathbf{a}_z)$$
 Evaluate the divergence of \mathbf{D} .
7. If $\mathbf{E} = \frac{16}{r} \cos 2\theta \mathbf{a}_\theta$. Evaluate the divergence of \mathbf{E} .
8. Let $\mathbf{D} = (2\rho z^2 \mathbf{a}_\rho + \rho \cos^2 \phi \mathbf{a}_z)$. Evaluate
 - (a) $\oint \mathbf{D} \cdot d\mathbf{S}$
 - (b) $\int \nabla \cdot \mathbf{D} dv$
 over the region defined by $0 \leq \rho \leq 5$, $0 < \phi < 2\pi$, $-1 \leq z \leq 1$.

Sheet ①

" Vectors Analysis "

Ex ①: given: vectors

$$\vec{M} = -10 \vec{a}_x + 4 \vec{a}_y - 8 \vec{a}_z$$

$$\vec{N} = 8 \vec{a}_x + 7 \vec{a}_y - 2 \vec{a}_z$$

Find: a) unit vector in $(-\vec{M} + 2\vec{N})$ direction.

b) $|5\vec{a}_x + \vec{N} - 3\vec{M}|$

c) $|\vec{M}| |\vec{N}| (\vec{M} + \vec{N})$

Solution

a) let: $\vec{A} = -\vec{M} + 2\vec{N}$

$$= 10 \vec{a}_x - 4 \vec{a}_y + 8 \vec{a}_z + 16 \vec{a}_x + 14 \vec{a}_y - 4 \vec{a}_z$$

$$= 26 \vec{a}_x + 10 \vec{a}_y + 4 \vec{a}_z$$

$$|\vec{A}| = \sqrt{(26)^2 + (10)^2 + (4)^2} = 28.142$$

$$\therefore \vec{a}_A = \frac{26 \vec{a}_x + 10 \vec{a}_y + 4 \vec{a}_z}{28.142} = \frac{\vec{A}}{|\vec{A}|}$$

$$= 0.923 \vec{a}_x + 0.355 \vec{a}_y + 0.142 \vec{a}_z$$

b) let: $\vec{B} = 5 \vec{a}_x + \vec{N} - 3\vec{M}$

$$= 5 \vec{a}_x + 8 \vec{a}_x + 7 \vec{a}_y - 2 \vec{a}_z$$

$$+ 30 \vec{a}_x - 12 \vec{a}_y + 24 \vec{a}_z$$

$$= 43 \vec{a}_x - 5 \vec{a}_y + 22 \vec{a}_z$$

$$\therefore |\vec{B}| = \sqrt{(43)^2 + (-5)^2 + (22)^2}$$

c) let $\vec{C} = |\vec{M}| |\vec{N}| (\vec{M} + \vec{N})$

Don't forget to check the units and the signs of the components.

$$c) |\vec{M}| = \sqrt{100 + 16 + 64} = 13.416$$

$$|\vec{N}| = \sqrt{64 + 49 + 4} = 10.8167$$

$$(\vec{M} + \vec{N}) = 2\vec{a}_x + 11\vec{a}_y - 10\vec{a}_z$$

$$\therefore C = 13.416 \times 10.8167 (2\vec{a}_x + 11\vec{a}_y - 10\vec{a}_z)$$

$$= -580.5\vec{a}_x + 3193\vec{a}_y - 2902\vec{a}_z$$

$$= (-580.5, 3193, 2902)$$

another form to represent vector ↙

Ex (2): given: Vectors

$$\vec{OA} : (0, 0, 0) \rightarrow (1, 2, 3) \Rightarrow \vec{a}_x + 2\vec{a}_y + 3\vec{a}_z$$

$$\vec{OB} : (0, 0, 0) \rightarrow (2, 3, -2) \Rightarrow 2\vec{a}_x + 3\vec{a}_y - 2\vec{a}_z$$

Find: a) $\vec{A}(\vec{A} - \vec{B})$

b) Unit vector in the direction of line

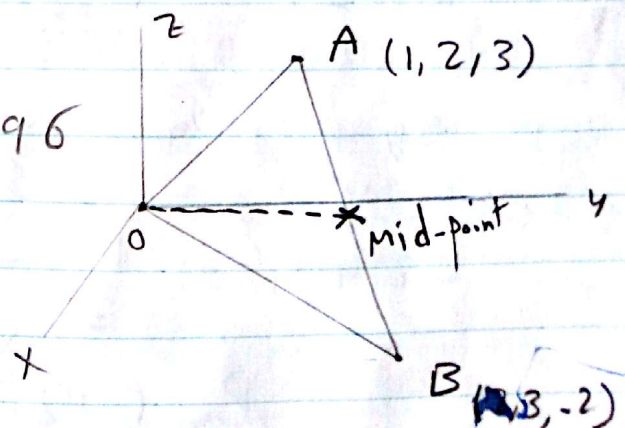
extending from $(0, 0, 0)$ to the mid point of the line joining the ends of A and B.

Solution

$$\vec{A} - \vec{B} = -\vec{a}_x - \vec{a}_y + 5\vec{a}_z$$

$$|\vec{A} - \vec{B}| = \sqrt{1 + 1 + 25} = 5.196$$

$$\therefore \vec{A}(\vec{A} - \vec{B}) = \frac{-\vec{a}_x - \vec{a}_y + 5\vec{a}_z}{5.196}$$



$$M = \frac{1}{2} (A + B) \leftarrow \text{mid-point} \in \frac{1}{2} (3, 5, 1)$$

$$\therefore \bar{M} = \left(3\bar{a}_x + 5\bar{a}_y + \bar{a}_z \right) \frac{1}{2}$$

$$\therefore |\bar{M}| = \sqrt{\quad} = 2.958$$

$$\begin{aligned} \therefore \bar{a}_{\bar{M}} &= \frac{\bar{M}}{|\bar{M}|} \\ &= 0.571 \bar{a}_x + 0.8457 \bar{a}_y + 0.169 \bar{a}_z \end{aligned}$$

Ex (3): given: $\bar{A} = (6, -2, -4)$, $\bar{a}_{AB} = (2, -2, 1)/3$
 $|\bar{AB}| = 10$ Find B ? (B_x, B_y, B_z)
Solution

$$\bar{AB} = |\bar{AB}| \bar{a}_{AB} = B - A$$

$$\frac{10}{3} (2, -2, 1) = (B_x - 6) \bar{a}_x + (B_y + 2) \bar{a}_y + (B_z + 4) \bar{a}_z$$

$$\therefore B_x - 6 = \frac{20}{3} \rightarrow B_x = 12.66$$

$$B_y + 2 = \frac{-20}{3} \rightarrow B_y = -8.66$$

$$B_z + 4 = \frac{10}{3} \rightarrow B_z = -0.66$$

$$\therefore B (12.66, -8.66, -0.66)$$

Ex [4]: given: Two vectors $\vec{A} = 2\vec{a}_x + \vec{a}_y + 3\vec{a}_z$
 $\vec{B} = \vec{a}_x - 3\vec{a}_y + 2\vec{a}_z$. Find: The acute angle
 using . dot product . Cross product
 Solution

$$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta = 2 + (-3) + 6$$

$$\sqrt{1+9+4} \times \sqrt{4+1+9} \cdot \cos \theta = 5$$

$$3.741 \times 3.741 \cos \theta = 5$$

$$\theta = \cos^{-1}(\quad) = 69.07^\circ$$

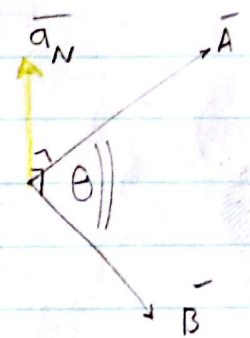
$$\vec{A} \times \vec{B} = |\vec{A}| |\vec{B}| \sin \theta \vec{a}_N = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ 2 & 1 & 3 \\ 1 & -3 & 2 \end{vmatrix}$$

$$3.741 \times 3.741 \sin \theta \vec{a}_N = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ 2 & 1 & 3 \\ 1 & -3 & 2 \end{vmatrix}$$

$$= 11\vec{a}_x - 4\vec{a}_y - 7\vec{a}_z$$

$$= |\vec{A} \times \vec{B}| \vec{a}_N$$

$$= \sqrt{11^2 + 4^2 + 7^2}$$



$$\therefore \theta = \sin^{-1}(\quad) = 69.07^\circ$$

Ex [5]: given: points $M(0.1, -0.2, -0.1)$
 $N(-0.2, 0.1, 0.3)$, $P(0.4, 0, 0.1)$
 Find: a) \vec{R}_{MN} b) $\vec{R}_{MN} \cdot \vec{R}_{MP}$
 c) Scalar projection of \vec{R}_{MN} on \vec{R}_{MP}
 d) angle betw \vec{R}_{MN} & \vec{R}_{MP}

Solution

→

$$a) \bar{R}_{MN} = N - M = (-0.3, 0.3, 0.4)$$

$$\bar{R}_{MP} = P - M = (0.3, 0.2, 0.2)$$

$$b) \bar{R}_{MN} \cdot \bar{R}_{MP} = -0.09 + 0.06 + 0.08 = 0.05$$

$$c) \text{ scalar projection of } \bar{R}_{MN} \text{ on } \bar{R}_{MP} = \bar{R}_{MN} \cdot \hat{a}_{\bar{R}_{MP}}$$

$$= |\bar{R}_{MN}| \cos \theta$$

$$= \frac{\bar{R}_{MN} \cdot \bar{R}_{MP}}{|\bar{R}_{MP}|}$$

$$= \frac{0.05}{0.412} = 0.1213$$

$$d) \rightarrow 0.583 \cos \theta = 0.1213$$

$$\therefore \theta = \cos^{-1} () = 78^\circ$$

Ex [6]: given: $\bar{F} = 10 \bar{a}_x - 6 \bar{a}_y + 5 \bar{a}_z$

a) Find vector component of \bar{F} that is parallel to $\bar{G} = 0.1 \bar{a}_x + 0.2 \bar{a}_y + 0.3 \bar{a}_z$.

b) " " " " F perpendicular = " G

c) " " " " G " = " F

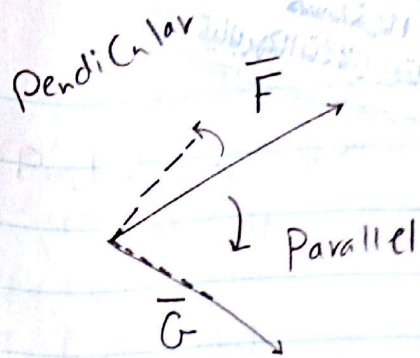
solution

$$\vec{F}_{\parallel G}$$

$$= (\vec{F} \cdot \vec{a}_G) \vec{a}_G$$

قيمة مقدار \vec{F} على \vec{G}

اتجاه المركبة الموازية لـ \vec{G}



$$\vec{a}_G = \frac{0.1\vec{a}_x + 0.2\vec{a}_y + 0.3\vec{a}_z}{0.5916} = \frac{0.1^2 + 0.2^2 + 0.3^2}{0.5916}$$

$$= (0.93, 1.86, 2.79)$$

$$\vec{F}_{\perp G} : \vec{F} = \vec{F}_{\parallel} + \vec{F}_{\perp}$$

$$\therefore \vec{F}_{\perp G} = \vec{F} - \vec{F}_{\parallel G}$$

$$= (9.07, -7.86, 2.21)$$

Ex(7): given, Three vectors

$$\vec{R}_1 = (7, 3, -2) \quad \vec{R}_2 = (-2, 7, 3)$$

$$\vec{R}_3 = (0, 2, 3)$$

a) \vec{a}_N ($\vec{R}_1 - \vec{R}_2$) and ($\vec{R}_2 - \vec{R}_3$)

b) \vec{a}_N \vec{R}_1 and \vec{R}_2

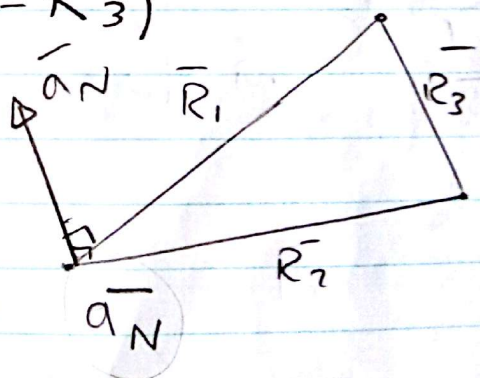
c) area of the triangle defined by \vec{R}_1, \vec{R}_2

a) $\vec{R}_1 \times \vec{R}_2$

$$= |\vec{R}_1| |\vec{R}_2| \sin \theta$$

$$= |\vec{R}_1 \times \vec{R}_2| \vec{a}_N$$

$$\therefore \vec{a}_N = \frac{\vec{R}_1 \times \vec{R}_2}{|\vec{R}_1 \times \vec{R}_2|} = \frac{5, 25, 55}{60.6} = (0.08, 0.41, 0.91)$$



$$b) \quad \vec{R}_1 - \vec{R}_2 = (9, -4, 1) = \vec{A}$$

$$\vec{R}_2 - \vec{R}_3 = (-2, 5, -6) = \vec{B}$$

$$\therefore \vec{A} \times \vec{B} = |\vec{A} \times \vec{B}| \vec{a}_{N_{AB}}$$

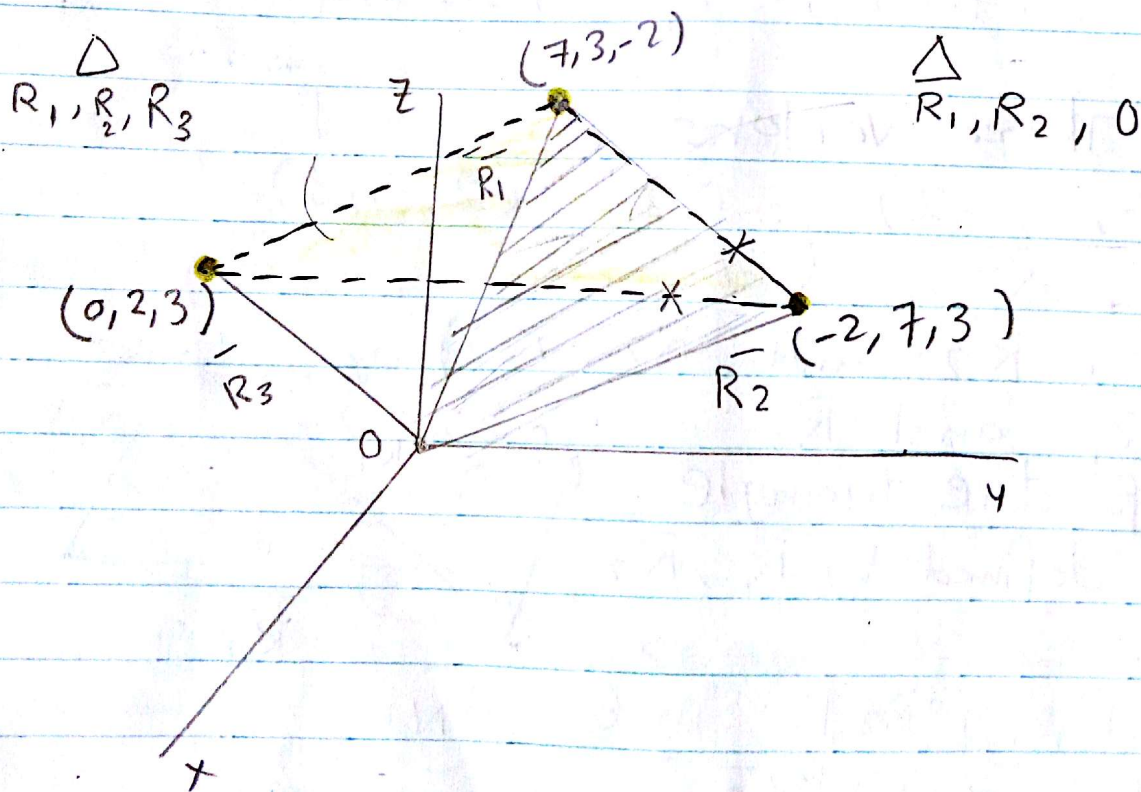
$$\vec{a}_{N_{AB}} = \frac{\vec{A} \times \vec{B}}{|\vec{A} \times \vec{B}|} = \frac{(19, 92, 32)}{63.95} = (0.3, 0.81, 0.5)$$

$$c) \quad \text{Area of } \triangle_{\vec{R}_1, \vec{R}_2} = \frac{1}{2} |\vec{R}_1 \times \vec{R}_2|$$

$$= 30.3$$

$$d) \quad \text{Area of } \triangle_{\vec{R}_1, \vec{R}_2, \vec{R}_3} = \frac{1}{2} |(\vec{R}_1 - \vec{R}_2) \times (\vec{R}_3 - \vec{R}_2)|$$

$$= 32$$

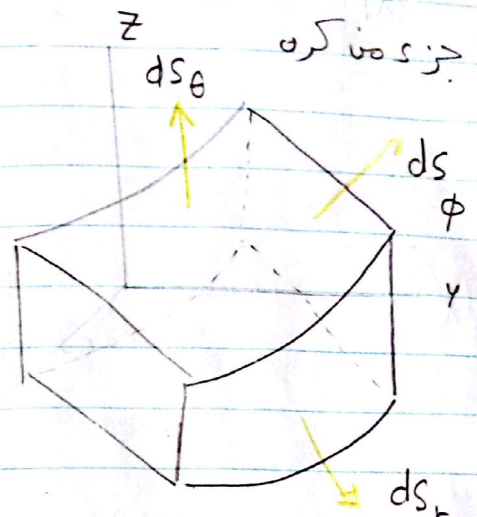


Ex(9) given: The surfaces
 $r=2, 4$, $\theta=30^\circ, 50^\circ$, $\phi=20^\circ, 60^\circ$
 identify a closed surface. Find:
 (a) Volume (b) A_{tot} (c) l (d) l_{largest}
 Solution

Spherical coordinates
 $dr, r d\theta, r \sin \theta d\phi$

$$(a) dv = r^2 \sin \theta dr d\theta d\phi$$

$$\begin{aligned} V &= \int dv \\ &= \int_{\phi=20}^{60} \int_{\theta=30}^{50} \int_{r=2}^4 dv \\ &= \left. \frac{r^3}{3} \right|_2^4 * \left. -\cos \theta \right|_{30}^{50} * \left. \phi \right|_{20 \times \frac{\pi}{180}}^{60 \times \frac{\pi}{180}} \\ &= 2.91 \rightarrow \text{check} \end{aligned}$$



$$\begin{aligned} (b) A &= \int ds \\ &= \int_{\phi=20}^{60} \int_{\theta=30}^{50} \int_{r=2}^4 r^2 \sin \theta dr d\theta d\phi + \int_{\phi=20}^{60} \int_{r=2}^4 r \sin \theta dr d\phi \\ &\quad + \int_{\theta=30}^{50} \int_{r=2}^4 r dr d\theta + \int_{\phi=20}^{60} \int_{\theta=30}^{50} r \sin \theta d\theta d\phi \\ &= 12.61 \end{aligned}$$

Ex 10 given: Point

(a) $r=2$, $\theta=1$ rad, $\phi=0.8$ rad

(b) $x=3$, $y=2$, $z=-1$

(c) $\rho=2.5$, $\phi=0.7$ rad, $z=1.5$

Express the unit vector \bar{a}_x in spherical components

Solution

From Table:

Unit vector

\bar{a}_x

Point

$$\bar{a}_x = \sin \theta \cos \phi \bar{a}_r + \cos \theta \cos \phi \bar{a}_\theta + (-\sin \phi) \bar{a}_\phi \rightarrow (*)$$

a) at $(2, 1 \text{ rad}, 0.8 \text{ rad}) \rightarrow \therefore \bar{a}_x = \checkmark$

b) Point $(x, y, z) \rightarrow$ Point (r, θ, ϕ)

$$r = \sqrt{x^2 + y^2 + z^2} = \sqrt{14}$$

$$\theta = \cos^{-1} \frac{z}{r} = 105.5^\circ$$

$$\phi = \tan^{-1} \left(\frac{y}{x} \right) = 33.7^\circ$$

$\therefore \bar{a}_x = \checkmark$

c) Point $(\rho, \phi, z) \rightarrow$ Point (r, θ, ϕ)

$$r = \sqrt{\rho^2 + z^2} = \sqrt{8.5}$$

$$\theta = \cos^{-1} \frac{z}{r} = 59^\circ$$

$$\phi = 0.7 \text{ rad}$$

$\therefore \bar{a}_x = \checkmark$

sheet ②

"Vector Algebra and Calculs"

Ex [1]: Find the volume defined by:
(a) $3 < r < 5$, $0.1\pi < \theta < 0.3\pi$, $1.2\pi < \phi < 1.6\pi$
(b) $4 < \rho < 6$, $2 < z < 5$, $30^\circ < \phi < 60^\circ$

Solution

(a) Using Spherical Coordinates (r, θ, ϕ)
 $dv = r^3 \sin \theta \, dr \, d\theta \, d\phi$

$$\begin{aligned} \therefore V &= \int_V dv = \int_{\phi=1.2\pi}^{1.6\pi} \int_{\theta=0.1\pi}^{0.3\pi} \int_{r=3}^5 dv \\ &= \left. \frac{r^3}{3} \right|_3^5 * \left. -\cos \theta \right|_{0.1\pi \times \frac{180}{\pi}}^{0.3\pi \times \frac{180}{\pi}} \left. \phi \right|_{1.2\pi}^{1.6\pi} = 14.91 \text{ unit}^3 \end{aligned}$$

(b) Using Cylindrical (ρ, ϕ, z)

$$dv = \rho \, d\rho \, d\phi \, dz$$

$$\begin{aligned} V &= \int_V dv = \int_{z=2}^5 \int_{\phi=30^\circ}^{60^\circ} \int_{\rho=4}^6 dv \\ &= \left. \frac{\rho^2}{2} \right|_4^6 * \left. \phi \right|_{30 \times \frac{\pi}{180}}^{60 \times \frac{\pi}{180}} * \left. z \right|_2^5 = 5\pi \end{aligned}$$

المساحة

Ex[2]: Find the area of

(a) surface of $\rho = 2m$, $0 \leq z \leq 5$, $30^\circ < \phi < 120^\circ$.

(b) strip $0 < \theta < \pi$ on a spherical shell of radius r .

Solution

قشرة كروية

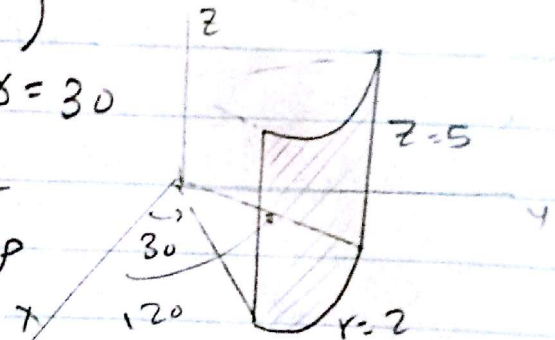
(a) $\therefore \rho$ const

$0 < \phi < 2\pi$

$$\bar{S}_\rho = \int_S dS_\rho = \int_{z=0}^5 \int_{\phi=30^\circ}^{120^\circ} \rho d\phi dz$$

$$\bar{S} = 5\pi m^2$$

\bar{a}_ρ



(b) $\therefore r$ const

$$\therefore \bar{S}_r = \int_S dS_r = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} r^2 \sin \theta d\theta d\phi$$

$$\bar{S}_r = 4\pi r^2 \bar{a}_r \rightarrow$$

مساحة كرة كاملة
وهذا متوقع

Ex 4] give vector \overline{AB}

A (2, 1, -3)

B (1, 3, 4)

Using (a) Cartesian

(b) cylindrical

(c) Spherical

solution

(a) Cartesian

$$\overline{AB} = \overline{B} - \overline{A}$$

$$= -\overline{a}_x + 2\overline{a}_y + 7\overline{a}_z$$

(b) Cylindrical

$$\overline{AB} = \overline{AB}_\rho \overline{a}_\rho + \overline{AB}_\phi \overline{a}_\phi + \overline{AB}_z \overline{a}_z$$

$$\overline{AB}_\rho = \overline{AB} \cdot \overline{a}_\rho = (-\overline{a}_x + 2\overline{a}_y + 7\overline{a}_z) \cdot \overline{a}_\rho$$

From Table

$$\overline{AB}_\rho = -\cos\phi + 2\sin\phi + 0$$

$$\overline{AB}_\phi = \overline{AB} \cdot \overline{a}_\phi = \sin\phi + 2\cos\phi + 0$$

$$\overline{AB}_z = 7$$

$$\therefore \overline{R}_{AB} = 2.236 \overline{a}_\phi + 7 \overline{a}_z$$

AT Point A

$$\phi = \tan^{-1} \frac{y}{x}$$

$$= 26.56^\circ$$

$$\rho = \sqrt{x^2 + y^2}$$

$$= \sqrt{5}$$

(c) Spherical

From Table

$$\overline{AB}_r = \overline{AB} \cdot \overline{a}_r = -5.61$$

$$\overline{AB}_\theta = \overline{AB} \cdot \overline{a}_\theta = -4.18$$

$$\overline{AB}_\phi = \overline{AB} \cdot \overline{a}_\phi = 2.236$$

AT A

$$\phi = \tan^{-1} \frac{y}{x}$$

$$= 26.56^\circ$$

$$\theta = \cos^{-1} \frac{z}{\rho}$$

$$= 143.3^\circ$$

$$\therefore \overline{AB} = -5.61 \overline{a}_r - 4.18 \overline{a}_\theta + 2.236 \overline{a}_\phi$$

Ex 5: Find the gradient of these scalar fields:

(a) $U = 4xz^2 + 3yz$

(b) $W = 2\rho(z^2+1) \cos \phi = 2\rho z^2 \cos \phi$

(c) $H = r^2 \cos \theta \cos \phi + 2\rho \cos \phi$

(نقطة) مشتقات

solution

gradient $\Rightarrow \nabla$ = \square \hat{a}_i

(a) $\nabla U = \frac{\partial U}{\partial x} \bar{a}_x + \frac{\partial U}{\partial y} \bar{a}_y + \frac{\partial U}{\partial z} \bar{a}_z$
(Cartesian)
 $= 4z^2 \bar{a}_x + 3z \bar{a}_y + (8xz + 3y) \bar{a}_z$

(b) $\nabla W = \frac{\partial W}{\partial \rho} \bar{a}_\rho + \frac{1}{\rho} \frac{\partial W}{\partial \phi} \bar{a}_\phi + \frac{\partial W}{\partial z} \bar{a}_z$
(Cylindrical)
 $= 2(z^2+1) \cos \phi \bar{a}_\rho + \frac{-1}{\rho} 2\rho(z^2+1) \bar{a}_\phi$
 $+ 4\rho \cos \phi \bar{a}_z$

(c) $\nabla H = \frac{\partial H}{\partial r} \bar{a}_r + \frac{1}{r} \frac{\partial H}{\partial \theta} \bar{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial H}{\partial \phi} \bar{a}_\phi$
(Spherical)
 $= 2r \cos \theta \cos \phi \bar{a}_r + \frac{1}{r} r^2 (-\sin \theta) \cos \phi \bar{a}_\theta$
 $+ \frac{1}{r \sin \theta} r^2 \cos \theta (-\sin \phi) \bar{a}_\phi$


Div. Theory:

$$\oint_V \nabla \cdot \vec{D} = \oint_S \vec{D} \cdot d\vec{s} = \int_V \nabla \cdot \vec{D} dv = \int_V (\nabla \cdot \vec{D}) dv$$

Ex [5]: given $2 < x, y, z < 3$

$$\vec{D} = \frac{2}{z^2} (yz \vec{a}_x + xz \vec{a}_y - 2xz \vec{a}_z)$$

Evaluate divergence of \vec{D} for the volume defined by $2 < x, y, z < 3$

Divergence. $\nabla \cdot$  = $\boxed{}$ $\vec{a}_x \vec{a}_y \vec{a}_z$

Solution

$$\nabla \cdot \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$

(Cartesian)

$$\vec{D} = \left(\frac{2y}{z} \right) \vec{a}_x + \left(\frac{2x}{z} \right) \vec{a}_y + \left(\frac{-4x}{z} \right) \vec{a}_z$$

D_x D_y $D_z = -4xz^{-1}$

$$\therefore \nabla \cdot \vec{D} = \text{Zero} + \text{Zero} + 4xz^{-2}$$
$$= \frac{4x}{z^2}$$

Ex [6]: given:

$$\vec{E} = 15\rho^2 \sin 2\phi \vec{a}_\rho + 20\rho^2 \cos 2\phi \vec{a}_\phi$$

Evaluate $\vec{\nabla} \cdot \vec{E}$? for the region
 $1 < \rho < 2\text{m}$, $1 < \phi < 2 \text{ rad}$, $1 < z < 2\text{m}$
 Solution.

$$\vec{\nabla} \cdot \vec{E} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho E_\rho) + \frac{1}{\rho} \frac{\partial E_\phi}{\partial \phi} + \frac{\partial E_z}{\partial z}$$

(Cylindrical)
 ρ dimension ϕ angle, z axis

Ex [7] given $\vec{E} = \frac{16}{r} \cos 2\theta \vec{a}_\theta$

Evaluate $\vec{\nabla} \cdot \vec{E}$ for $1 < r < 2$, $1 < \phi < 2$, $1 < \theta < 2$
 Solution

$$\vec{\nabla} \cdot \vec{E} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 E_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta E_\theta) + \frac{1}{r \sin \theta} \frac{\partial E_\phi}{\partial \phi}$$

(Spherical)
 r dimension θ angle ϕ angle

$$= \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \left(\frac{16}{r} \right) \cos 2\theta \right)$$

$$= \frac{16}{r^2 \sin \theta} \left\{ \sin \theta (-2 \sin 2\theta) + \cos 2\theta \cos \theta \right\}$$

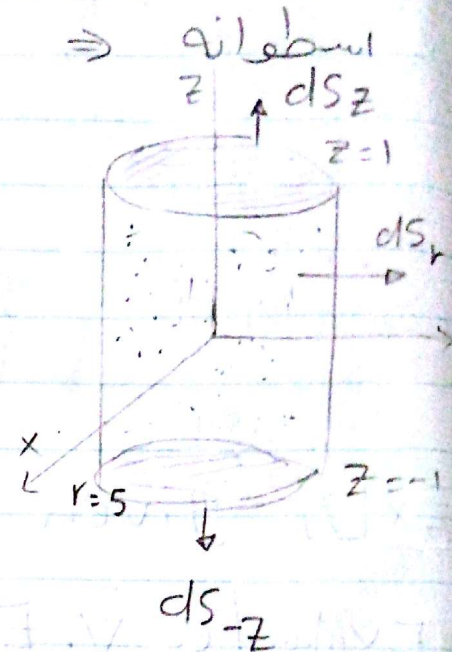
$$= \frac{16}{r^2} \left\{ -2 \sin 2\theta + \cos 2\theta \frac{\cos \theta}{\sin \theta} \right\}$$

Ex 8 given: $\vec{D} = 2\rho z^2 \vec{a}_\rho + \rho \cos^2 \phi \vec{a}_z$
 Evaluate: (a) $\oint_S \vec{D} \cdot d\vec{s}$

(b) $\int_V \nabla \cdot \vec{D} dv$
 over the region defined by:

$$0 \leq \rho \leq 5, 0 \leq \phi < 2\pi, -1 \leq z \leq 1 \Rightarrow$$

Solution
 $d\rho, \rho d\phi, dz$



(a) $\oint_S \vec{D} \cdot d\vec{s}$

$$= \int_{z=-1}^{z=1} \int_{\phi=0}^{2\pi} \int_{\rho=0}^5 + \int_{z=-1}^{z=1} \int_{\phi=0}^{2\pi} \int_{\rho=0}^5 + \int_{\phi=0}^{2\pi} \int_{\rho=0}^5 \int_{z=-1}^{z=1}$$

$$= - \int_{\phi=0}^{2\pi} \int_{\rho=0}^5 \int_{z=-1}^{z=1} (\rho \cos^2 \phi) (\rho d\rho d\phi dz) \quad (z=-1)$$

$$+ \int_{\phi=0}^{2\pi} \int_{\rho=0}^5 \int_{z=-1}^{z=1} (\rho \cos^2 \phi) (\rho d\rho d\phi dz) \quad (z=1)$$

$$= \frac{200\pi}{3}$$

(b) $\nabla \cdot \vec{D} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho)$

$$= \frac{1}{\rho} \frac{\partial}{\partial \rho} (2\rho^2 z^2) = \frac{1}{\rho} \rho 4z^2$$

$$= \int_{z=-1}^1 \int_{\phi=0}^{2\pi} \int_{\rho=0}^5 4z^2 \rho \, d\rho \, d\phi \, dz$$

$$= \left. \frac{4z^3}{3} \right|_{-1}^1 * \left. \frac{\rho^2}{2} \right|_0^5 * 2\pi$$

From (a) & (b)

$$= \frac{200\pi}{3}$$

Verification of Div. Theor ✕ #

$$\oint \vec{D} \cdot d\vec{s} = \int_V (\nabla \cdot \vec{D}) \, dV$$

surface integral

Volume integral



1. A 20 nC point charge is located at P (2, 4, -3) in free space. **Find**
 - (a) $\mathbf{E}(\mathbf{r})$.
 - (b) \mathbf{E} at A (-3, 2, 0).
2. Point charges $Q_1 = 5 \mu\text{C}$ and $Q_2 = -4 \mu\text{C}$ are placed at (3, 2, 1) and (-4, 0, 6), respectively.
Determine the force on Q_1 .
3. Point charges Q_1 and Q_2 are, respectively, located at (4, 0, -3) and (2, 0, 1). If $Q_2 = 4 \text{ nC}$, **Find** Q_1 such that
 - (a) The \mathbf{E} at (5, 0, 6) has no z-component
 - (b) The force on a test charge at (5, 0, 6) has no x-component.
4. **Determine** the total charge
 - (a) On line $0 < x < 5 \text{ m}$ if $\rho_l = 12x^2 \text{ mC/m}$
 - (b) On the cylinder $\rho = 3, 0 < z < 4 \text{ m}$ if $\rho_s = \rho z^2 \text{ nC/m}^2$
 - (c) Within the sphere $r = 4 \text{ m}$ if $\rho_v = \frac{10}{r \sin \theta} \text{ C/m}^3$
5. A line charge density ρ_l is uniformly distributed over a length of $2a$ with centre as origin along x axis. **Find** \mathbf{E} at a point P which is on z axis at a distance d.
6. It is required to hold four equal point charges each in equilibrium at the corners of square. **Find** the point charge which will do this, if placed at the centroid of the square.
7. A ring placed along $y^2 + z^2 = 4, x = 0$ carries a uniform charge of $5 \mu\text{C/m}$.
 - (a) **Find** \mathbf{E} at P (3, 0, 0).
 - (b) If two identical point charges Q are placed at (0, -3, 0) and (0, 3, 0) in addition to the ring,
Find the value of Q such that $\mathbf{E} = 0$ at P.
8. A sheet of charges $\rho_s = 2 \text{ nC/m}^2$, is present at the plane $x = 3$ in free space, and a line charge $\rho_l = 2 \text{ nC/m}$ is located at $x = 1, z = 4$. Find
 - (a) The magnitude of electric field intensity at the origin.
 - (b) The direction of \mathbf{E} at p (4, 5, 6).
 - (c) What is the force per meter length on the line charge?
9. A point charge 100 pC is located at (4, 1, -3) while the x-axis carries charge 2 nC/m . If the plane $z = 3$ also carries charge 5 nC/m^2 , **Find** \mathbf{E} at (1, 1, 1).

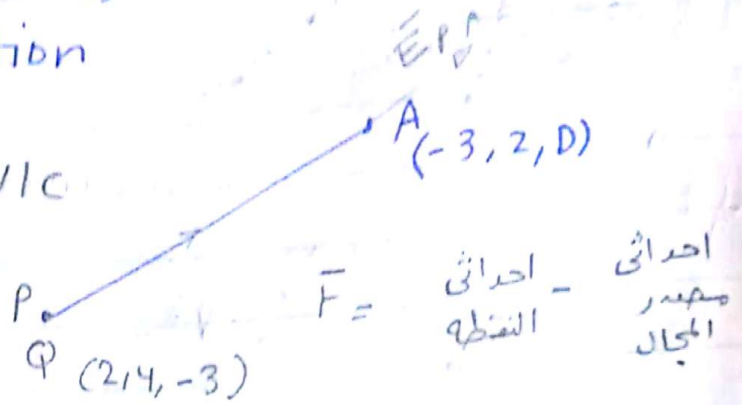
Sheet ③

Ex ①: given: $Q = 20 \text{ nC}$ at $P(2, 4, -3)$
Required a) $E(r)$ b) E at $A(-3, 2, 0)$

Solution

a) $\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \vec{a}_r$ N/C

$\vec{E} = \frac{20 \times 10^{-9}}{4\pi\epsilon_0 r^2} \vec{a}_r$



b) at $A(-3, 2, 0)$

$\vec{r}_{PA} = A - P = -5\vec{a}_x - 2\vec{a}_y + 3\vec{a}_z$

$|\vec{r}_{PA}| = 6.164$

$\vec{E} = -3.84\vec{a}_x - 1.53\vec{a}_y + 2.30\vec{a}_z$

Ex ③: given: Q_1 at $(4, 0, -3)$ A

Q_2 at $B(2, 0, 1)$, $= 4 \text{ nC}$

Find Q_1 ? such that:

a) \vec{E}_z at $C(5, 0, 6) = \text{Zero}$

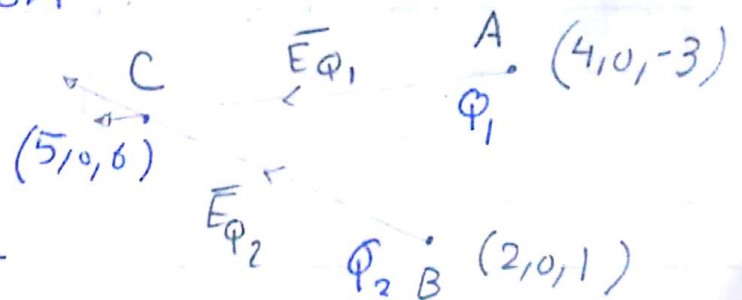
b) \vec{F}_x on Q at $(5, 0, 6) = \text{Zero}$
test charge

Solution

$\vec{E}_{\text{tot}} = \vec{E}_{Q_1} + \vec{E}_{Q_2}$

$= \frac{Q_1}{4\pi\epsilon_0 R_{AC}^3} \vec{R}_{AC}$

$+ \frac{Q_2}{4\pi\epsilon_0 R_{BC}^2} \vec{R}_{BC}$



$$\vec{R}_{AC} = C - A = 3\vec{a}_x + 9\vec{a}_z, |\vec{R}_{AC}| = \sqrt{82}$$

$$\vec{R}_{BC} = C - B = 3\vec{a}_x + 5\vec{a}_z, |\vec{R}_{BC}| = \sqrt{34}$$

$$\vec{E}_{tot} = \frac{1}{4\pi\epsilon_0} \left[\left(\frac{Q_1}{82\sqrt{82}} + \frac{3 \times 4 \times 10^{-9}}{34\sqrt{34}} \right) \vec{a}_x + \left(\frac{9Q_1}{82\sqrt{82}} + \frac{5 \times 4 \times 10^{-9}}{34\sqrt{34}} \right) \vec{a}_z \right]$$

for $E_z = \text{Zero}$

$E_z \rightarrow (*)$

$$\therefore \frac{9Q_1}{82\sqrt{82}} = -\frac{5 \times 4 \times 10^{-9}}{34\sqrt{34}}$$

$$\therefore Q_1 = -8.32 \text{ nC}$$

for $F_x = \text{Zero}$ on test charge q

$$\therefore F_x = \text{Zero} \Rightarrow \therefore E_x = \frac{F_x}{q} = \text{Zero}$$

nm $(*)$

$$\therefore \frac{Q_1}{82\sqrt{82}} = -\frac{3 \times 4 \times 10^{-9}}{34\sqrt{34}}$$

$$\therefore Q_1 = -0.499 \text{ nC}$$

$$Q = \int \rho_v dV$$

$$a) Q = \int \rho_l dl = \int_{x=0}^5 12x^2 dx$$

$$= \frac{12x^3}{3} \Big|_0^5 = 0.5 C$$

$$b) Q = \int \int \rho_s ds = \int_0^4 \int_0^{2\pi} \int_0^3 \rho z^2 \rho d\phi dz$$

$$= \rho \frac{z^3}{3} \Big|_0^4 * \phi \Big|_0^{2\pi} \Big|_0^3$$

$$= 1.206 MC$$

$$c) Q = \int \int \int \rho_v dv$$

$$= \int_{\theta=0}^{\pi} \int_{\phi=0}^{2\pi} \int_{r=0}^4 \frac{10}{r \sin \theta} r^2 \sin \theta dr d\theta d\phi$$

$$10 * \frac{r^2}{2} \Big|_0^4 * \theta \Big|_0^{\pi} * \phi \Big|_0^{2\pi}$$

$$= 157.9 C$$

Ex ②: given: $Q_1 = 5 \mu C$ at $(3, 2, 1)$
 $Q_2 = -4 \mu C$ at $(-4, 0, 6)$
 Find F_{Q_1} ? solution

$$\vec{F} = \frac{Q_1 Q_2}{4\pi\epsilon R^2} \vec{a}_R = \frac{Q_1 Q_2}{4\pi\epsilon R^3} \vec{R}$$

Q_1 \vec{F}_{Q_1}
 $(3, 2, 1)$

$$\vec{R} = \vec{r}_1 - \vec{r}_2$$

21/

$$= 7\vec{a}_x + 2\vec{a}_y - 5\vec{a}_z$$

Q_2 $(-4, 0, 6)$

$\vec{R} =$ احداثى مصدر الشحنة - احداثى الشحنة المستهدفة

$$|\vec{R}| = \sqrt{78}$$

$$\vec{F}_{Q_1} = \frac{5 \times 10^{-6} \times -4 \times 10^{-6}}{4\pi \times 8.85 \times 10^{-12} (\sqrt{78})^3} \vec{R}$$

$\vec{F}_{2,1}$ القوة المؤثرة على Q_1 نتيجة Q_2

$$(7\vec{a}_x - 2\vec{a}_y - 5\vec{a}_z)$$

$$= -1.827\vec{a}_x - 0.522\vec{a}_y + 1.31\vec{a}_z \text{ mN}$$

Ex ④: given

- a) $\rho_L = 12x^2 \text{ C/m}$ for $0 < x < 5$
 b) $\rho_s = 3z^2 \text{ nC/m}^2$ for $0 \leq z < 4$
 c) $\rho_v = \frac{10}{r \sin\theta} \text{ C/m}^3$, $r = 4$

solution

$$\vec{E}_{\text{tot}} = \frac{Q}{4\pi\epsilon_0 r_+^2} \vec{a}_{r_+} + \frac{Q}{4\pi\epsilon_0 r_-^2} \vec{a}_{r_-}$$

$$\vec{r}_+ = -3\vec{a}_y + 3\vec{a}_z \quad r = \sqrt{18}$$

$$\vec{r}_- = 3\vec{a}_y + 3\vec{a}_z$$

$$\vec{E}_{\text{tot}} = \frac{Q}{4\pi\epsilon_0 \sqrt[3]{18}} 6 \vec{a}_z$$

$$\frac{-0.32}{\cancel{\epsilon_0}} = \frac{6Q}{4\pi\cancel{\epsilon_0} \sqrt[3]{18}}$$

$$\therefore Q = -51.1 \mu\text{C}$$

Ex 7: given

Ring $z=0$
 $y^2 + x^2 = 4$

$\rho_L = 5 \text{ nC/m}$

Find a) $\vec{E}_P(0,0,3)$

b) $Q? \Rightarrow E_{tot P} = \text{Zero}$

Solution

a)

$$E = \int \frac{\rho_L dl}{4\pi\epsilon_0 R^2} \vec{a}_R$$

For symmetry $\vec{E}_P = \text{Zero} \therefore \vec{E} = \vec{E}_z$

$$\therefore \vec{E} = \frac{5 \times 10^{-6} \times 2 \times 3}{2 \times 4\pi \epsilon_0 (13)^{3/2}}$$

$$|\vec{R}| = \sqrt{13}$$

$$\vec{R} = -2\vec{a}_x + 3\vec{a}_z$$

$$dl = a d\phi$$

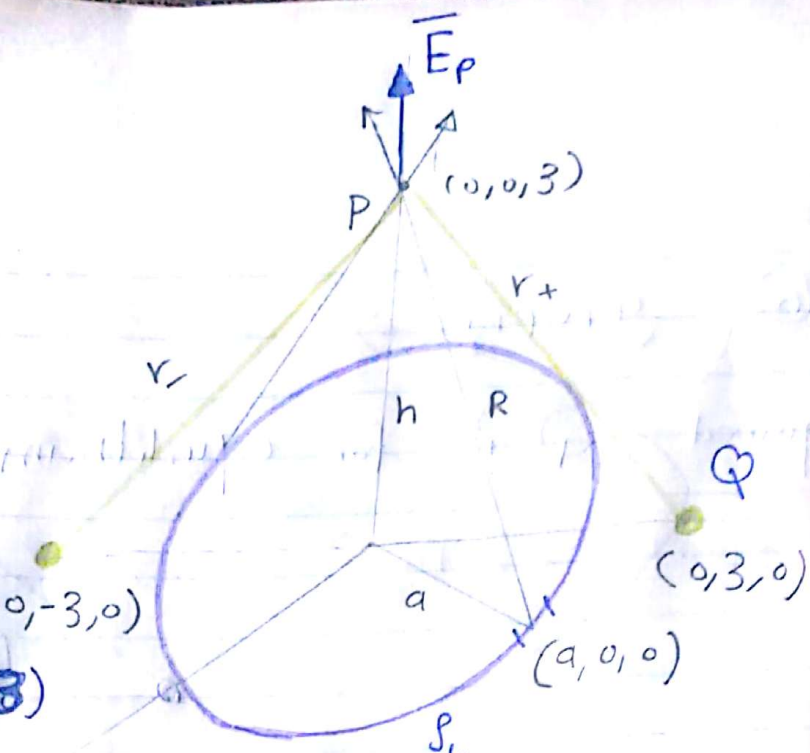
$$\int_0^{2\pi} d\phi \vec{a}_z$$

$$\vec{E}_{\text{Ring}} = \frac{0.32}{\epsilon_0} \text{ MN/C}$$

b) $E_{tot} = \text{Zero}$

$$= E_{\text{Ring}} + E_{Q_{tot}}$$

$$= E_{\text{Ring}} + \vec{E}_{+r} + \vec{E}_{-r}$$





Electrical Power and Machines Depart. Electromagnetic Fields

Sheet (4)



Tanta University

Gauss's law and Electric flux density

Faculty of Engineering

1. A point charge $Q = 100 \mu\text{C}$ is located at the origin. **Determine** the total flux passing through the following surfaces:
 - (a) A hemisphere of radius 2m defined by $0 \leq \theta \leq 0.5\pi$, $0 \leq \phi \leq 2\pi$, $r = R_A$
 - (b) A spherical shell defined by $\theta_1 \leq \theta \leq \theta_2$
2. Cylindrical surfaces at $r = 2$, 4 , and 6m carry uniform charge densities of 20 , -4 , and $\rho_{so} \text{ nC/m}^2$ respectively. **Find**
 - (a) \mathbf{D} at $r = 1$, 3 , and 5 m
 - (b) **How much** electric flux passes through the closed surface $\rho = 8 \text{ m}$, $0 < z < 1$?
 - (c) ρ_s such that $\mathbf{D} = 0$ at $r = 7 \text{ m}$.

3. Given that

$$\rho_v = \begin{cases} 12\rho \text{ nC/m}^3, & 1 < \rho < 2 \\ 0, & \text{otherwise} \end{cases}$$

Determine \mathbf{D} everywhere.

4. The Cylindrical surfaces at $\rho = 1$, 2 , and 3m carry uniform surface charge densities of 20 , -8 , and 5 nC/m^2 respectively.
 - (a) **How much** electric flux passes through the closed surface $\rho = 5$, $0 < z < 1$?
 - (b) **Find \mathbf{D}** at $\rho = 1$, 3 , and 5 m .

5. Let

$$\rho_v = \begin{cases} \frac{10}{r^2} \text{ mC/m}^3, & 1 < r < 4 \\ 0, & r > 0 \end{cases}$$

- (a) Find the net flux crossing surface $r = 2 \text{ m}$ and $r = 6 \text{ m}$.
 - (b) **Determine \mathbf{D}** at $r = 1 \text{ m}$ and $r = 5 \text{ m}$.
6. A uniform volume of $80 \mu\text{C/m}^3$, is present throughout the region $8\text{mm} < r < 10\text{mm}$. Let $\rho_v = 0$ for $0 < r < 8\text{mm}$. **Find**
 - (a) The total charge inside the spherical surface $r = 10\text{mm}$.
 - (b) \mathbf{D}_r at $r = 10\text{mm}$.
 - (c) If there is no charge for $r > 10\text{mm}$, find \mathbf{D}_r at $r = 20\text{mm}$.
7. In the region of free space that includes the volume, $2 < x, y, z < 3$,

$$\mathbf{D} = \frac{2}{z^2} (yz \mathbf{a}_x + xz \mathbf{a}_y - 2xz \mathbf{a}_z) \text{ C/m}^2.$$
 - (a) **Evaluate** the volume integral side of the divergence theorem for the volume defined by $2 < x, y, z < 3$.
 - (b) **Evaluate** the surface integral side for the corresponding closed surface.



8. If $\mathbf{D} = (15 \rho^2 \sin 2\phi \mathbf{a}_\rho + 20 \rho^2 \cos 2\phi \mathbf{a}_\phi) \text{ C/ m}^2$. Evaluate both sides of the divergence theorem for the region $1 < \rho < 2\text{m}$, $1 < \phi < 2\text{rad}$, $1 < z < 2\text{m}$.
9. If $\mathbf{D} = \frac{16}{r} \cos 2\theta \mathbf{a}_\theta \text{ C/ m}^2$. Use two different methods to find Q_{tot} within the region $1 < r < 2\text{m}$, $1 < \phi < 2\text{rad}$, $1 < \theta < 2\text{rad}$.



Electrical Power and Machines Depart. Electromagnetic Fields

Sheet (4)



Tanta University

Gauss's law and Electric flux density

Faculty of Engineering

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 - (b) A spherical shell defined by $\theta_1 \leq \theta \leq \theta_2$
2. Cylindrical surfaces at $r = 2$, 4 , and 6m carry uniform charge densities of 20 , -4 , and $\rho_{so} \text{ nC/m}^2$ respectively. **Find**
 - (a) \mathbf{D} at $r = 1$, 3 , and 5 m
 - (b) **How much** electric flux passes through the closed surface $\rho = 8 \text{ m}$, $0 < z < 1$?
 - (c) ρ_s such that $\mathbf{D} = 0$ at $r = 7 \text{ m}$.

3. Given that

$$\rho_v = \begin{cases} 12\rho \text{ nC/m}^3, & 1 < \rho < 2 \\ 0, & \text{otherwise} \end{cases}$$

Determine \mathbf{D} everywhere.

4. The Cylindrical surfaces at $\rho = 1$, 2 , and 3m carry uniform surface charge densities of 20 , -8 , and 5 nC/m^2 respectively.
 - (a) **How much** electric flux passes through the closed surface $\rho = 5$, $0 < z < 1$?
 - (b) **Find \mathbf{D}** at $\rho = 1$, 3 , and 5 m .

5. Let

$$\rho_v = \begin{cases} \frac{10}{r^2} \text{ mC/m}^3, & 1 < r < 4 \\ 0, & r > 0 \end{cases}$$

- (a) Find the net flux crossing surface $r = 2 \text{ m}$ and $r = 6 \text{ m}$.
 - (b) **Determine \mathbf{D}** at $r = 1 \text{ m}$ and $r = 5 \text{ m}$.
6. A uniform volume of $80 \mu\text{C/m}^3$, is present throughout the region $8\text{mm} < r < 10\text{mm}$. Let $\rho_v = 0$ for $0 < r < 8\text{mm}$. **Find**
 - (a) The total charge inside the spherical surface $r = 10\text{mm}$.
 - (b) \mathbf{D}_r at $r = 10\text{mm}$.
 - (c) If there is no charge for $r > 10\text{mm}$, find \mathbf{D}_r at $r = 20\text{mm}$.
7. In the region of free space that includes the volume, $2 < x, y, z < 3$,

$$\mathbf{D} = \frac{2}{z^2} (yz \mathbf{a}_x + xz \mathbf{a}_y - 2xz \mathbf{a}_z) \text{ C/m}^2.$$
 - (a) **Evaluate** the volume integral side of the divergence theorem for the volume defined by $2 < x, y, z < 3$.
 - (b) **Evaluate** the surface integral side for the corresponding closed surface.



8. If $\mathbf{D} = (15 \rho^2 \sin 2\phi \mathbf{a}_\rho + 20 \rho^2 \cos 2\phi \mathbf{a}_\phi) \text{ C/m}^2$. Evaluate both sides of the divergence theorem for the region $1 < \rho < 2\text{m}$, $1 < \phi < 2\text{rad}$, $1 < z < 2\text{m}$.
9. If $\mathbf{D} = \frac{16}{r} \cos 2\theta \mathbf{a}_\theta \text{ C/m}^2$. Use two different methods to find Q_{tot} within the region $1 < r < 2\text{m}$, $1 < \phi < 2\text{rad}$, $1 < \theta < 2\text{rad}$.

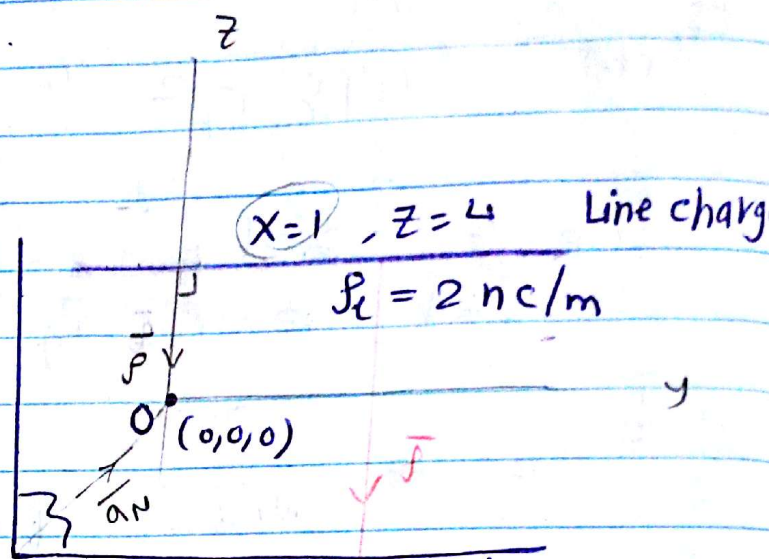
EX 8: given:

Find,

a) $|\vec{E}|$ at origin, $|\vec{E}_0|$

b) \vec{E}_p , $P(4, 5, 6)$

c) F/ρ on line charge



Solution

$$a) \vec{E}_{tot} = \vec{E}_{\rho_L} + \vec{E}_{\rho_S}$$

$$= \frac{\rho_L}{2\pi\epsilon_0 r^2} \vec{r} + \frac{\rho_S}{2\epsilon_0} \vec{a}_N$$

$$\vec{r} = (0, 0, 0) - (1, 5, 4) = (-1, 0, -4)$$

$$r = \sqrt{17}$$

$$\vec{a}_N = -\vec{a}_x$$

$$\therefore \vec{E}_{tot} = \frac{2 \times 10^{-9}}{2\pi\epsilon_0 (17)} (-1, 0, -4) + \frac{2 \times 10^{-9}}{2\epsilon_0} (-1, 0, 0)$$

$$= -115 \vec{a}_x + 8.45 \vec{a}_z$$

$$|\vec{E}_0| = \sqrt{\quad} = 115.31 \text{ N/C}$$

$$\vec{E}_{\text{tot}} = \frac{Q}{4\pi\epsilon_0 r_+^2} \vec{a}_{r_+} + \frac{Q}{4\pi\epsilon_0 r_-^2} \vec{a}_{r_-}$$

$$\vec{r}_+ = -3\vec{a}_y + 3\vec{a}_z \quad r = \sqrt{18}$$

$$\vec{r}_- = 3\vec{a}_y + 3\vec{a}_z$$

$$\therefore \vec{E}_{\text{tot}} = \frac{Q}{4\pi\epsilon_0 \sqrt[3]{18}} 6\vec{a}_z$$

$$\frac{-0.32}{\cancel{\epsilon_0}} = \frac{6Q}{4\pi\cancel{\epsilon_0} \sqrt[3]{18}}$$

$$\therefore Q = -51.1 \mu\text{C}$$

$$b) \vec{P} = (4, 5, 6) - (1, 4, 4) = (3, 0, 2)$$

$$|\vec{P}| = \sqrt{15}$$

$$\vec{a}_N = + \vec{a}_x$$

$$\therefore \vec{E}_P = 120.13 \vec{a}_x + 4.79 \vec{a}_z$$

c)

المجال المتواجد فيه الشحنة ← \vec{E} ← القوة المؤثرة على شحنة
 الشحنة المدروسة ← $\vec{F} = q \vec{E}$

الشحنة المدروسة ← خط الشحنت

$$q = q_s l$$

مصدر المجال = مصدر القوة ← سطح الشحنت

$$\vec{E}_{P_s} = \frac{q_s}{2\epsilon_0} \vec{a}_N$$

$$\vec{a}_N = -\vec{a}_x$$

$$\frac{F}{l} = q_s \frac{q_s}{2\epsilon_0} - \vec{a}_x$$

$$= 2.27 \times 10^{-7} \text{ N/m}$$

Ex 9: given:

$$Q = 100 \text{ pC at } (4, 1, -3)$$

$$\rho_L = 2 \text{ nC/m on } x\text{-axis } (y=0, z=0)$$

$$\rho_s = 5 \text{ nC/m}^2 \text{ on } \underline{z}\text{-plane at } \underline{z} = 3$$

Find:

$$\underline{E} \rightarrow (1, 1, 1)$$

A solution

$$\underline{E}_{\text{tot}} = \frac{Q}{4\pi\epsilon_0 R^3} \underline{\bar{R}} + \frac{\rho_L}{2\pi\epsilon_0 \rho^2} \underline{\bar{\rho}} + \frac{\rho_s}{2\epsilon_0} \underline{\bar{a}}_N$$

$$\underline{\bar{R}} = (1, 1, 1) - (4, 1, -3) = (-3, 0, 4)$$

$$\underline{\bar{\rho}} = (1, 1, 1) - (1, 0, 0) = (0, 1, 1)$$

$$\underline{\bar{a}}_N = -\underline{\bar{a}}_z \quad \begin{matrix} z_{\rho_s} > z_{\text{point}} \end{matrix}$$

$$\begin{aligned} &= \frac{100 \times 10^{-12}}{4\pi\epsilon_0 (25)^{3/2}} (-3, 0, 4) + \frac{2 \times 10^{-9}}{2\pi\epsilon_0 (2)} (0, 1, 1) \\ &\quad + \frac{5 \times 10^{-9}}{2\epsilon_0} (0, 0, -1) \end{aligned}$$

Ex ①: Given Q at $(0,0,0)$

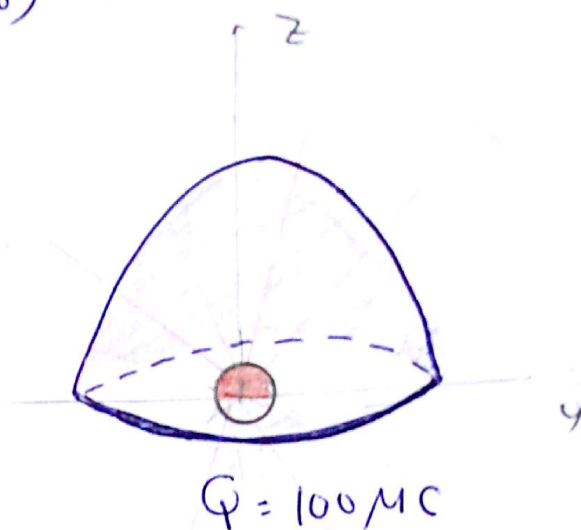
Find ψ_{tot}

a) hemisphere, $r=2$

$$0 \leq \theta \leq \pi/2, \quad 0 \leq \phi \leq 2\pi$$

b) Spherical shell

$$\theta_1 \leq \theta \leq \theta_2, \quad r=R$$



Solution

$$a) \quad \psi = \oint \vec{D}_r \cdot d\vec{S}_r = Q_{enc} = Q/2 \quad (\text{From Gauss})$$

$$\vec{D}_r = \frac{Q}{4\pi\epsilon_0 r^2} \vec{a}_r, \quad d\vec{S}_r = r^2 \sin\theta d\theta d\phi \vec{a}_r$$

$$\therefore \psi = \frac{Q}{4\pi\epsilon_0 r^2} \int_0^{2\pi} \int_0^{\pi/2} \sin\theta d\theta d\phi$$

$$\psi = \frac{Q}{2} = 50 \mu\text{wb}$$

$$b) \quad \psi = \frac{Q}{4\pi\epsilon_0 r^2} \int_0^{2\pi} \int_{\theta_1}^{\theta_2} \sin\theta d\theta d\phi$$

$$(\cos\theta_1 - \cos\theta_2) 2\pi$$

$$= \frac{Q}{2} (\cos\theta_1 - \cos\theta_2)$$

$$\psi = 50 (\cos\theta_1 - \cos\theta_2) \mu\text{wb}$$

X(2): Given: cylindrical surfaces

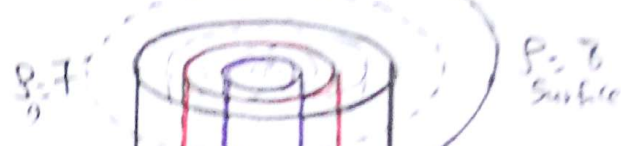
Req: a) \vec{D} at
 $\rho = 1, 3, 5 \text{ m}$

b) ψ pass

$\rho_{s3} = 9 \text{ nC/m}^2$, $\rho = 8 \text{ m}$, $0 < z < 1$

c) $\rho_s \rightarrow D = 0$

$\rho = 7 \text{ m}$



$\rho = 2$, $\rho_{s1} = 20 \text{ nC/m}^2$ خواص سطح جاورس

$\rho_{s2} = -4 \text{ nC/m}^2$

$\rho = 6$

$\rho_s = \rho_{s0} ?$

1 - سطح مغلف

2 - سطح متماثل حول المحور

3 - غير بالنقطه المحاوره

solution

Gauss law

$$\oint \vec{D} \cdot d\vec{s} = Q_{enc}$$

الشحنه الكليه الموجوده داخل سطح جاورس

كانه الجار الكليه سطح جاورس

a) at $\rho_g = 1 \text{ m} \rightarrow Q_{enc} = \text{Zero} \therefore D = 0$

at $\rho_g = 3 \text{ m} \rightarrow Q_{enc} = Q_1 = \rho_{s1} A_1 = 2\pi \rho_{s1} L \rho_{s1}$

$$\oint \vec{D} \cdot d\vec{s} = D \int \int r d\phi dz = D (2\pi \rho_g L)$$

$\phi = 0$ $z = 0$

$$\therefore D (2\pi \rho_g L) = \rho_{s1} 2\pi \rho_{s1} L$$

$$\therefore \vec{D} = \frac{2 \times 20 \times 10^{-9}}{3} = 13.3 \times 10^{-9} \vec{a}_r \text{ wb/m}^2$$

at $\rho_g = 5 \text{ m} \rightarrow Q_{enc} = Q_1 + Q_2 = \rho_{s1} A_1 + \rho_{s2} A_2$

$$= 2\pi L (\rho_{s1} \rho_{s1} + \rho_{s2} \rho_{s2})$$

$$\oint \vec{D} \cdot d\vec{s} = D (2\pi \rho_g L)$$

$$\therefore D = \frac{2 \times 20 \times 10^{-9} - 4 \times 4 \times 10^{-9}}{5} = 4.8 \times 10^{-9} \vec{a}_r \text{ wb/m}^2$$

$$\begin{aligned}
 b) \quad \therefore \Psi &= Q_{enc} = \oint \vec{D}_s \cdot d\vec{S}_s \quad ? \\
 &= Q_1 + Q_2 + Q_3 \\
 &= 2\pi l (\rho_1 \rho_{s1} + \rho_2 \rho_{s2} + \rho_3 \rho_{s3}) \\
 &= 2\pi \times 1 \times 10^{-9} (2 \times 20 - 4 \times 4 + 6 \times 4) \\
 &= 3.76 \times 10^{-7} \text{ wb}
 \end{aligned}$$

c) ρ_{s0} ? From Gauss

$$\begin{aligned}
 \oint \vec{D} \cdot d\vec{S} &= Q_{enc} = 2\pi l (\rho_1 \rho_{s1} + \rho_2 \rho_{s2} + \rho_3 \rho_{s0}) \\
 \cancel{D} (2\pi \rho_s l) &= (2 \times 20 \times 10^{-9} - 4 \times 4 \times 10^{-9} + 6 \rho_{s0}) \\
 \therefore \rho_{s0} &= -4 \text{ nC/m}^2
 \end{aligned}$$

Ex ③: Given: $\rho_v = \begin{cases} 128 \text{ nC/m}^3 & 1 < \rho < 2 \\ 0 & \text{otherwise} \end{cases}$

Determine \vec{D} everywhere.

Solution

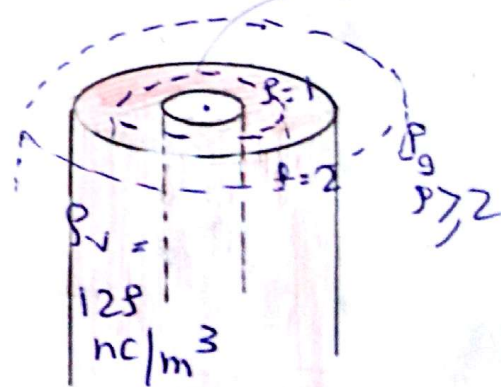
everywhere

$\rho < 1$	$1 < \rho < 2$	$\rho > 2$
$Q_{enc} = \text{Zero}$	$Q_{enc} = Q_{vol}$	$Q_{enc} = Q_{tot}$

$\therefore \vec{D} = \text{Zero}$
 $\rho < 1$

$\vec{D} ?$

$\vec{D} ?$



Ex (3) $1 \leq \rho < 2$

$$Q_{enc} = \int_V \rho_v dv = \int_0^L \int_0^{2\pi} \int_1^{\rho_g} 12 \rho^2 d\rho d\phi dz$$

$$= 12 \left. \frac{\rho^3}{3} \right|_{\rho=1}^{\rho_g} * 2\pi * L = \frac{8\pi L}{4} (\rho_g^3 - 1) \rightarrow \textcircled{1}$$

$$\oint \vec{D} \cdot d\vec{S}_\rho = D_\rho \int_0^L \int_0^{2\pi} \rho_g d\phi dz$$

$$= D (2\pi \rho_g L) \rightarrow \textcircled{2}$$

$$\therefore \bar{D} = \frac{4(\rho_g^3 - 1)}{\rho_g} \bar{a}_\rho$$

$0 < \rho_g < \rho$

$\rho_{7/2}$

$$Q_{enc} = Q_{tot} = \int_0^L \int_0^{2\pi} \int_1^2 12 \rho^2 d\rho d\phi dz$$

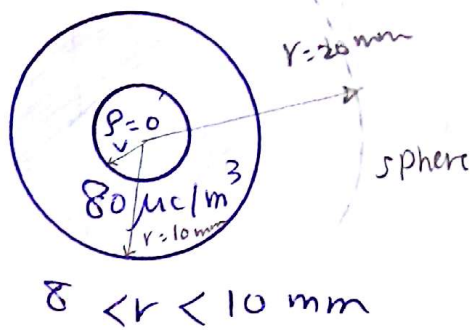
$$= 8\pi L (2^3 - 1^3) = \frac{56\pi L}{28}$$

$$\oint \vec{D} \cdot d\vec{S}_\rho = D (2\pi \rho_g L)$$

$$\bar{D} = \frac{28}{\rho_g} \bar{a}_\rho$$

$\rho_{7/2}$

Ex 6: given.



Find: a) Q_{tot} inside sphere $r=10mm$

b) \vec{D}_r at $r=10mm$

c) \vec{D}_r at $r=20mm$

if $Q=0$ for $r > 10mm$

a) $Q_{tot} = \cancel{Q_{r \rightarrow 8}} + Q_{8 \rightarrow 10} = \int_0^{2\pi} \int_0^{\pi} \int_8^{10} \rho_v r^2 \sin\theta dr d\theta d\phi$ (Solution $r=10$)

$$= \rho_v \left. \frac{r^3}{3} \right|_8^{10} (2)(2\pi) = 5.45 \text{ PC}$$

b) From Gauss at $r=10mm$

$$\oint \vec{D}_r \cdot d\vec{S}_r = Q_{enc}$$

$$\vec{D}_r \int_0^{2\pi} \int_0^{\pi} r^2 \sin\theta d\theta d\phi$$

$$\phi=0 \quad \theta=0 \quad (4\pi r^2)$$

$$\therefore \vec{D}_r = \frac{Q_{enc}}{4\pi r^2} = \frac{5.45 \times 10^{-12}}{4\pi (10 \times 10^{-3})^2} \vec{a}_r$$

$$= 4.4 \times 10^{-9} \vec{a}_r \text{ wb/m}^2$$

c) at $r=20mm$

$$\vec{D}_r = \frac{5.45 \times 10^{-12}}{4\pi (20 \times 10^{-3})^2} \vec{a}_r$$

$$= 1.102 \times 10^{-9} \vec{a}_r \text{ wb/m}^2$$



1. **Find** the work done in carrying a 5 C charge from P (1, 2, -4) to R (3, -5, 6) in electric field

$$\mathbf{E} = \mathbf{a}_x + z^2 \mathbf{a}_y + 2yz \mathbf{a}_z \text{ V/m}$$

2. In free space, $V = x^2 y (z + 3) \text{ V}$. **Find**
 (a) \mathbf{E} at (3, 4, -6)
 (b) **The charge** within the cube $0 < x, y, z < 1$
3. Using cylindrical coordinates, **Find** the work done in carrying a unit positive charge from $P_1(a, 0, 0)$ to $P_2(\frac{a}{\sqrt{2}}, \frac{a}{\sqrt{2}}, 0)$ in electric field

$$\mathbf{E} = (r \sin \phi \cos \phi + z \cos \phi) \mathbf{a}_\phi \text{ V/m}$$
4. Let $V = 2xy^2z^2 \text{ V}$ in free space. Evaluate each of the following quantities at P (3, 2, -1):
 (a) V ; (b) \mathbf{E} ; (c) $|\mathbf{E}|$; (d) \mathbf{a}_N ; (e) \mathbf{D} .
5. Given the potential field $V = 80 r^2 \cos \theta \text{ V}$ and a point P (2.5, 30, 60) in free space, **Find** at P:
 (a) V ; (b) \mathbf{E} ; (c) \mathbf{D} ; (d) ρ_v ; (e) \mathbf{a}_N .
6. Given a surface charge density of 8 nC/m^2 on the plane $x = 2$, a line charge density of 30 nC/m on the line $x = 1, y = 2$ and $1 \mu\text{C}$ point charge at P (-1, -1, 2). **Find** V_{AB} for points A (3, 4, 0) and B (4, 0, 1).
7. A uniform volume charge density $\rho_v \text{ C/m}^3$ is present throughout a sphere with radius R. **Find** both \mathbf{E} and V inside and outside the sphere. Note that there is no charge for $r > R$.
8. A finite line with uniformly distributed line charge density C/m . The line is located with centre as origin along z-axis. **Find** V and \mathbf{E} at a point P with a distance r from the center of the line.

Sheet (4)

$$\vec{D} = \left(\frac{2y}{z}\right) \vec{a}_x + \left(\frac{2x}{z}\right) \vec{a}_y + \left(\frac{-4x}{z}\right) \vec{a}_z$$

$$\boxed{7} \quad \vec{D} = \frac{2}{z^2} (yz \vec{a}_x + xz \vec{a}_y - 2xz \vec{a}_z)$$

Req. \rightarrow Vol. integral $\int_V \rho_v dv$ $2 < x, y, z < 3$
 \rightarrow Surface integral $\oint \vec{D} \cdot d\vec{s}$

Solution.

Volume

$$\rho_v = \nabla \cdot \vec{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$
$$= \text{zero} + \text{zero} + \frac{4x}{z^2} = \frac{4x}{z^2}$$

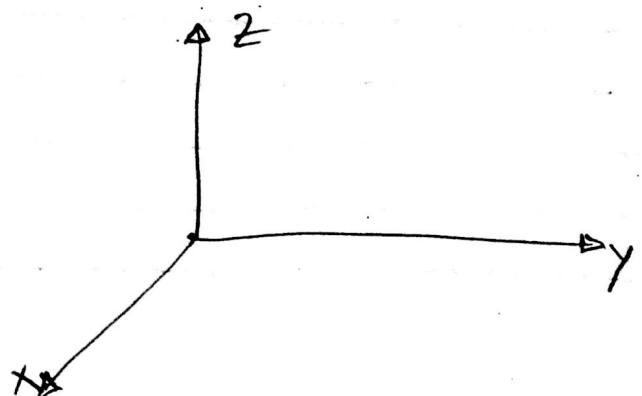
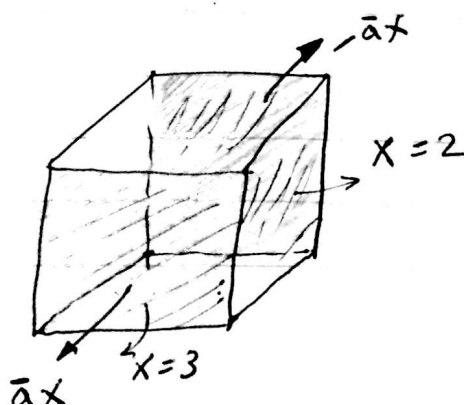
$$\int_V \rho_v dv = \int_{z=2}^3 \int_{y=2}^3 \int_{x=2}^3 \frac{4x}{z^2} dx dy dz$$
$$= \int_2^3 dy * \int_2^3 4x dx * \int_2^3 z^{-2} dz$$
$$= (3-2) * 2x^2 \Big|_2^3 * \frac{z^{-1}}{-1} \Big|_2^3$$

$$= 1 * 2(9-4) * -1 \left(\frac{1}{3} - \frac{1}{2} \right)$$
$$= 0.833 * 2 = 1.667$$

Surface integral

$\oint \vec{D} \cdot d\vec{s}$

$d\vec{s} =$

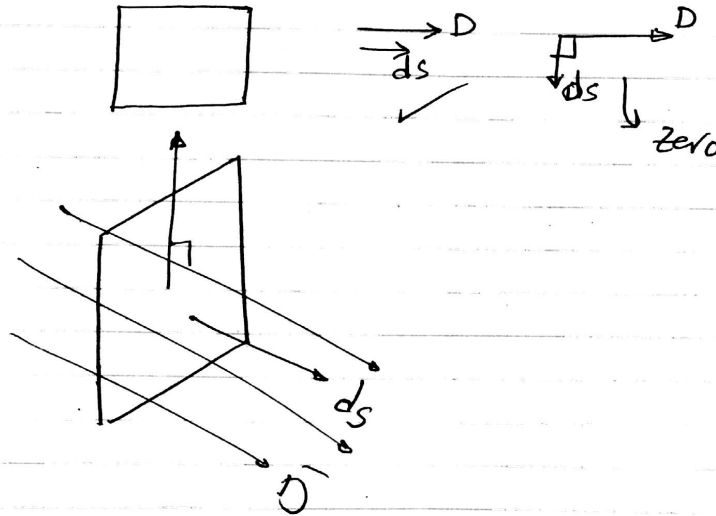


المساحة $\oplus \leftarrow$ العبر الكبير
 $\ominus \leftarrow$ العبر الصغير

$$ds \begin{cases} \rightarrow dx dy (\pm \bar{a}_z) \\ \rightarrow dx dz (\pm \bar{a}_y) \\ \rightarrow dy dz (\pm \bar{a}_x) \end{cases}$$

$x=3$
 $x=2$

ملاحظة كل مساحة سيغير من علامته D التي لها نفس الاتجاه موجة مساحة



$$\oint D \cdot ds$$

سطح مغلق
المكعب

$$\textcircled{1} \int_{x=2} \bar{D} \cdot \bar{ds}_x$$

$$= \int \frac{2}{z^2} (\underbrace{yz \bar{a}_x + xz \bar{a}_y}_{\bar{D}_x} - \cancel{2xz \bar{a}_z}) \cdot dy dz \bar{a}_x$$

$$= \int_{x=2} \bar{D}_x \cdot \bar{ds}_x$$

نبدأ مع باقي الأسطح.

على الوجه السليم لا كعجب

$$\oint D \cdot ds = \int_1 + \int_2 + \int_3 + \int_4 + \int_5 + \int_6$$

$$\textcircled{1} \int_{x=2} -D_x dy dz = \int_{z=2}^3 \int_{y=2}^3 -\frac{2y}{z} dy dz$$

$$= -y^2 \Big|_2^3 * \ln z \Big|_2^3$$

$$\textcircled{2} \int_{x=3} D_x dy dz = y^2 \Big|_2^3 * \ln z \Big|_2^3$$

$$\textcircled{3} \int_{y=2} -D_y dx dz = - \int_{z=2}^3 \int_{x=2}^3 \frac{2x}{z} dx dz$$

$$\textcircled{4} \int_{y=3} D_y dx dz = \int \int \frac{2x}{z} dx dz$$

$$\textcircled{5} \int_{z=2} -D_z dx dy = - \int_2^3 \int_2^3 \frac{-4x}{2} dx dy$$

$$= \int \int 2x dx dy = x^2 \Big|_2^3 y \Big|_2^3$$

$$= (9-4)(3-2) = 5$$

$$\textcircled{6} \int_{z=3} D_z dx dy = \int_2^3 \int_2^3 \frac{-4x}{3} dx dy = \frac{-2x^2}{3} \Big|_2^3 y \Big|_2^3$$

$$= \frac{-2(9-4)}{3} * 1 = \frac{-10}{3}$$

$$\oint D \cdot ds = 5 + \left(\frac{-10}{3}\right) = 1.667 \text{ C} \quad \#$$

Ex 9 $\vec{D} = \frac{16}{r} \cos 2\theta \hat{a}_\theta \text{ C/m}^2$

Sol. $1 < r < 2$, $1 < \phi < 2 \text{ rad}$, $1 < \theta < 2$
 $Q_{\text{tot}} \rightarrow$ two methods

Solution

method ①: $Q_{\text{tot}} = \int_{\text{Vol.}} (\nabla \cdot \vec{D}) dV$

$$\nabla \cdot \vec{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 D_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta D_\theta) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} (D_\phi)$$

$$= \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{16}{r} \cos 2\theta \right)$$

$$= \frac{16}{r^2 \sin \theta} \left\{ \sin \theta (-2 \sin 2\theta) + \cos 2\theta \cos \theta \right\}$$

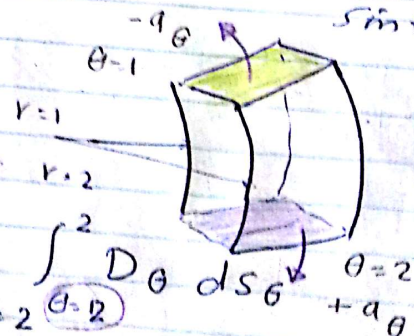
$$= \frac{16}{r^2} \left\{ -2 \sin 2\theta + \cos 2\theta \frac{\cos \theta}{\sin \theta} \right\}$$

method ②

$$Q_{\text{tot}} = \oint \vec{D} \cdot d\vec{s}$$

$$= \int_{\theta=1}^2 \int_{r=1}^2 -D_\theta d\theta dr + \int_{r=1}^2 \int_{\theta=1}^2 D_\theta d\theta dr + \int_{\theta=1}^2 \int_{r=1}^2 D_\phi d\theta dr + \int_{r=1}^2 \int_{\theta=1}^2 D_\phi d\theta dr$$

$$ds_\theta = r \sin \theta dr d\theta$$



9) $\bar{D} = \frac{16}{r} \cos 2\theta \sin \theta \text{ C/m}^2$

Find: $1 < r < 2$, $1 < \phi < 2 \text{ rad}$, $1 < \theta < 2 \text{ rad}$
 $Q_{\text{tot}} \rightarrow$ two methods

solution

method ①: $Q_t = \int (\nabla \cdot \bar{D}) dV$

$$\nabla \cdot \bar{D} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \bar{D}_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta \bar{D}_\theta) + \frac{1}{r \sin \theta} \frac{\partial \bar{D}_\phi}{\partial \phi}$$

$$= \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{16}{r} \cos 2\theta \right)$$

$$= \frac{16}{r^2 \sin \theta} \left\{ \sin \theta * (-2 \sin 2\theta) + \cos 2\theta \cos \theta \right\}$$

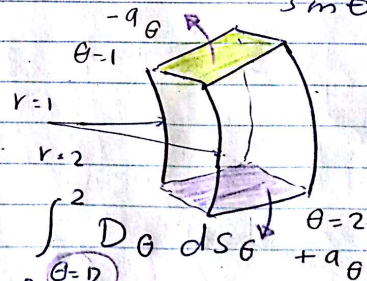
$$= \frac{16}{r^2} \left\{ -2 \sin 2\theta + \cos 2\theta \frac{\cos \theta}{\sin \theta} \right\}$$

method ②

$$Q_{\text{tot}} = \oint \bar{D} \cdot d\bar{s}$$

$$= \int_{\phi=0}^2 \int_{\theta=1}^2 -\bar{D}_\theta ds_\theta + \int_{\theta=0}^2 \int_{r=2}^1 \bar{D}_r ds_r + \int_{\theta=0}^2 \int_{r=1}^2 \bar{D}_r ds_r + \int_{\phi=0}^2 \int_{\theta=1}^2 \bar{D}_\phi ds_\phi$$

$$ds_\theta = r \sin \theta dr d\phi$$



#

Sheet (5)

Sheet ⑤

Ex ①: given: $Q = 5 \text{ C}$

$$\vec{E} = \vec{a}_x + z^2 \vec{a}_y + 2yz \vec{a}_z \text{ V/m}$$

Req: $W_{P \rightarrow R}$

$P(1, 2, -4)$

$R(3, -5, 6)$

Solution
Final

$$W_{P \rightarrow R} = - \oint_{\text{initial}} \vec{E} \cdot d\vec{L}$$

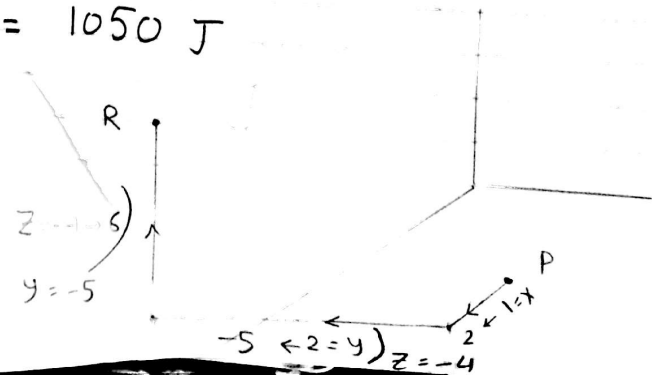
$$= 5 \int (\vec{a}_x + z^2 \vec{a}_y + 2yz \vec{a}_z) \cdot (dx \vec{a}_x + dy \vec{a}_y + dz \vec{a}_z)$$

$$= 5 \left(\int_1^3 dx + \int_2^{-5} z^2 dy + \int_{-4}^6 2yz dz \right)$$

$$= 5 \left(x \Big|_1^3 + z^2 y \Big|_2^{-5} + 2y \frac{z^2}{2} \Big|_{-4}^6 \right)$$

$$= 5 (2 + 16(-7) + (-5)(36 - 16))$$

$$W = 1050 \text{ J}$$



Ex 3

Ex ③: given $\vec{E} = (\rho \sin \phi \cos \phi - z \cos \phi) \vec{a}_\phi$
 $Q = 1 \text{ C}$

Find $W_{P_1 \rightarrow P_2}$ $P_1 (a, 0, 0)$

Using Cylindrical Coordinates
Solution

$$W = -Q \int_{int}^{fin} \vec{E} \cdot d\vec{L}$$

$P_2 (\frac{a}{\sqrt{2}}, \frac{a}{\sqrt{2}}, 0)$

$$P_1 (a, 0, 0) \rightarrow (\rho, \phi, z) \rightarrow (a, 0, 0)$$

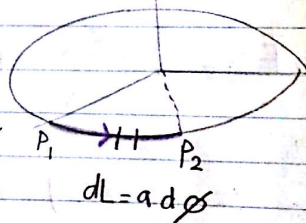
$$\rho = \sqrt{a^2 + 0} = a, \quad \phi = \tan^{-1} \frac{0}{a} = 0$$

$$P_2 (\frac{a}{\sqrt{2}}, \frac{a}{\sqrt{2}}, 0) \rightarrow (\rho, \phi, z) \rightarrow (a, \frac{\pi}{4}, 0)$$

$$\rho = \sqrt{(\frac{a}{\sqrt{2}})^2 + (\frac{a}{\sqrt{2}})^2} = a, \quad \phi = \tan^{-1} \frac{a/\sqrt{2}}{a/\sqrt{2}} = \frac{\pi}{4}$$

$$\therefore W = - \int \vec{E}_\phi \cdot d\vec{L}_\phi$$

$$= - \int_0^{\pi/4} r \left(\sin \phi \cos \phi - z \cos \phi \right) a d\phi$$



$$= -a^2 \int_0^{\pi/4} \sin \phi \cos \phi d\phi$$

$$= -a^2 \int_0^{\pi/4} \frac{1}{2} \sin 2\phi d\phi = -\frac{a^2}{2} \left(-\frac{\cos 2\phi}{2} \right) \Big|_0^{\pi/4}$$

$$W = -\frac{a^2}{4} \text{ J}$$

$$\sin 2\phi = 2 \sin \phi \cos \phi$$

قسط (2)

II

CH 6 Steady magnetic field

Biot-Savart's law

$$d\vec{H}_p = \frac{I d\vec{l} \times \vec{R}}{4\pi R^3} = \frac{I dL \sin\alpha}{4\pi R^2}$$

\vec{R} = المسافة بين العنصر $d\vec{l}$ والنقطة P

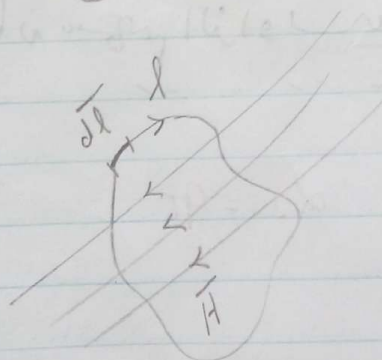
$$\vec{H} = \frac{I}{4\pi} \int \frac{d\vec{l} \times \vec{R}}{R^3}$$

$$\vec{B} = \mu \vec{H}$$

Ampere's circuital law

$$\oint \vec{H} \cdot d\vec{l} = \sum I$$

حساب المجال المغناطيسي الناتج عن تيار مستمر



\overline{E} ۵۴۵۵

اکرم و سائید

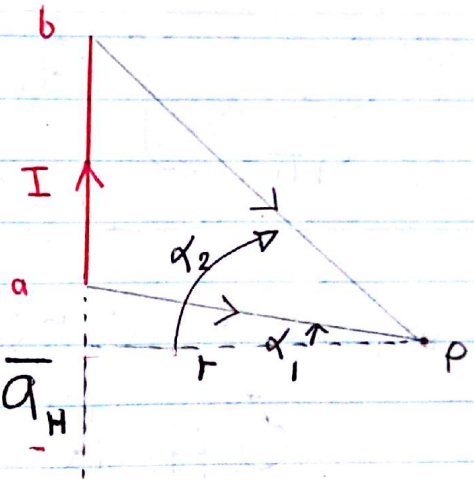
تخصر له بد اسه (شائبر) كوفى لاختنا السكته

Electromagnetic waves
تأثير كهربی (\vec{E})
تأثير مغناطیس (\vec{H})

For finite line.

$$\vec{a}_H = \vec{a}_I \times \vec{a}_r$$

$$\therefore H_p = \frac{I}{4\pi r} (\sin \alpha_2 - \sin \alpha_1) \bar{a}_H$$



البعد العمودي من نقطة

* لحدید اشارہ الزوايا

- إذا كان سهم الزاوية مع سهم لتيار ← الزاوية (+) للموصل
- " " " " " " ← " " (-)

For infinit line $\alpha_1 = -90$, $\alpha_2 = 90$

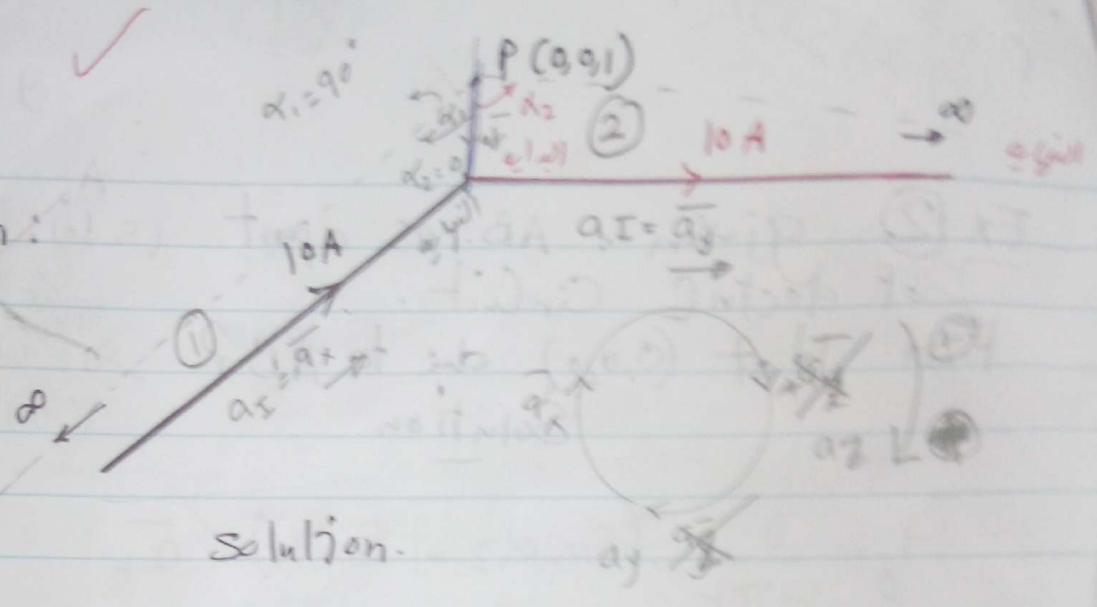
$$\therefore H_p = \frac{I}{2\pi r} a_r$$

3, 4

3

Ex 1 given:

Find H_p ?



Solution.

$$\vec{H} = \frac{I}{4\pi r} (\sin \alpha_2 - \sin \alpha_1) \vec{a}_H$$

For Part ①:

$$\alpha_1 = -90$$

$$\alpha_2 = 0$$

$$\begin{aligned} \vec{a}_H &= \vec{a}_I \times \vec{a}_r \\ &= -\vec{a}_x \times -\vec{a}_z \\ &= +\vec{a}_y \end{aligned}$$

$$|\vec{r}| = 1, I = 10A$$

$$\therefore H_{p1} = \frac{10}{4\pi(1)} \vec{a}_y$$

For Part ②:

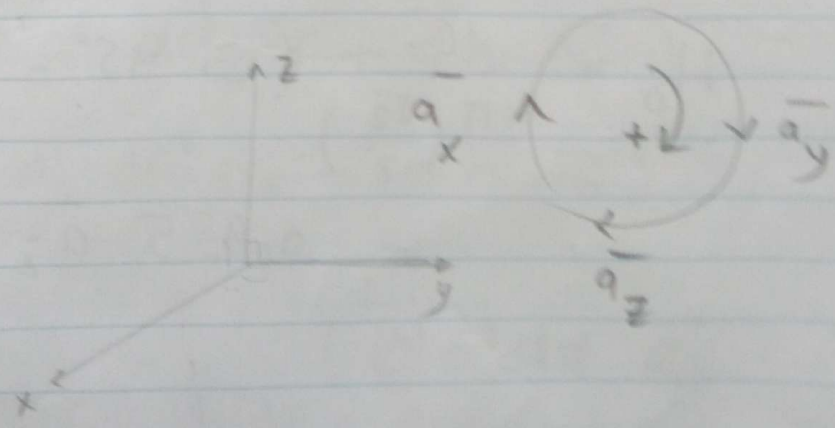
$$\alpha_1 = 0$$

$$\alpha_2 = 90$$

$$\begin{aligned} \vec{a}_H &= \vec{a}_I \times \vec{a}_r \\ &= \vec{a}_y \times -\vec{a}_z \\ &= -(-\vec{a}_x) = +\vec{a}_x \end{aligned}$$

$$H_{p2} = \frac{I}{4\pi(1)} \vec{a}_x$$

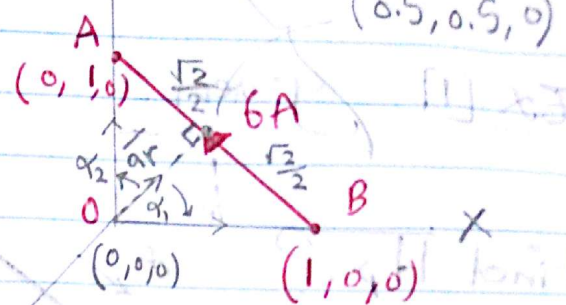
$$\therefore H_p = \frac{10}{4\pi} (\vec{a}_y + \vec{a}_x) \text{ A/m}$$



Ex ② given: AB as a part
of electric circuit.

Find H at $(0,0,0)$ due to AB?

Solution



$$\vec{H}_0 = \frac{I}{4\pi r} (\sin \alpha_2 - \sin \alpha_1) \vec{a}_H$$

$$\alpha_1 = -45^\circ$$

$$\alpha_2 = 45^\circ$$

$$r = \sqrt{(1)^2 - \left(\frac{\sqrt{2}}{2}\right)^2} = \frac{\sqrt{2}}{2}$$

$$\vec{a}_H = \vec{a}_I \times \vec{a}_r$$

$$\vec{a}_I = ? = \frac{\vec{I}}{|\vec{I}|} = \frac{(0, 1, 0) - (1, 0, 0)}{\sqrt{2}} = \frac{-\vec{a}_x + \vec{a}_y}{\sqrt{2}}$$

$$\vec{a}_r = ? = \frac{\vec{r}}{|\vec{r}|} = \frac{(\frac{1}{2}, \frac{1}{2}, 0) - (0, 0, 0)}{\sqrt{(\frac{1}{2})^2 + (\frac{1}{2})^2}} = \frac{\frac{\sqrt{2}}{2}(\vec{a}_x + \vec{a}_y)}{\sqrt{2}/2}$$

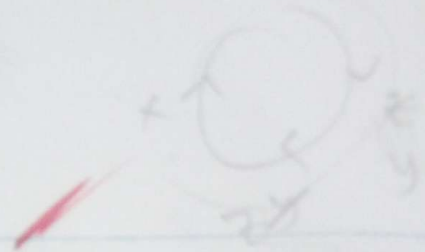
$$\therefore \vec{a}_H = \frac{1}{\sqrt{2}} \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ -1 & 1 & 0 \\ 1 & 1 & 0 \end{vmatrix} = \vec{a}_z$$

$$\vec{H}_0 = \frac{6}{4\pi \left(\frac{\sqrt{2}}{2}\right)} (\sin 45^\circ - \sin(-45^\circ)) \vec{a}_z$$

$$= 0.955 \vec{a}_z \text{ A/m}$$

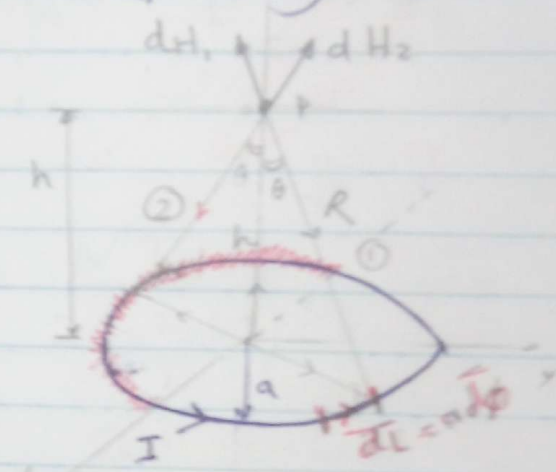
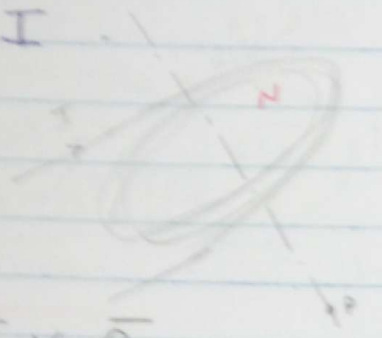
5

8



3 Sheet (6)

Required: The magnetic field intensity H on the axis of a circular ring due to current I .



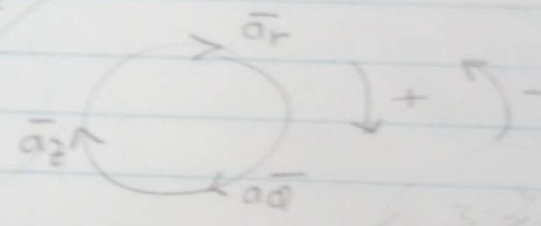
$$d\vec{H} = \frac{I d\vec{l} \times \vec{R}}{4\pi R^3}$$

For ① Use the same $0 \rightarrow \pi$

$$d\vec{l} = a d\phi \vec{a}_\phi$$

$$\vec{R} = -a \vec{a}_r + h \vec{a}_z$$

$$R = \sqrt{h^2 + a^2}$$



$$d\vec{l} \times \vec{R} = (-a^2 d\phi \vec{a}_z) \boxed{+} ah \vec{a}_r$$

For ② as the same Use the same $\pi \rightarrow 0$

$$d\vec{l} \times \vec{R} = a^2 d\phi \vec{a}_z \boxed{-} ah \vec{a}_r$$

$$dH_1 = \frac{I}{4\pi R^3} (a^2 d\phi \vec{a}_z + ah \vec{a}_r)$$

$$dH_2 = \frac{I}{4\pi R^3} (a^2 d\phi \vec{a}_z - ah \vec{a}_r)$$

$$\therefore dH_{\text{net}} = \frac{I}{4\pi (a^2 + h^2)^{3/2}} (2a^2 d\phi \vec{a}_z)$$

sheet [6]

① required: magnetic field intensity H on the axis of a circular loop (Current in 1A)

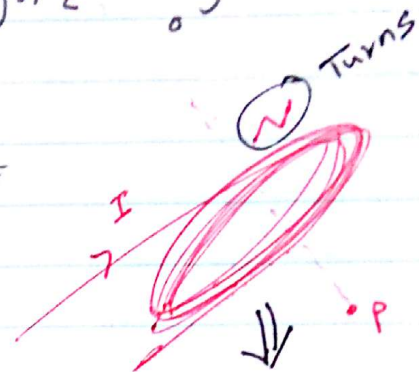
6 ~~3~~

$$H = \int_{\phi=0}^{\pi} dH = \frac{I}{4\pi} (2a^2) \int_0^{\pi} d\phi \frac{1}{(a^2+h^2)^{3/2}}$$

$$= \frac{I 2a^2 \pi}{4\pi (a^2+h^2)^{3/2}} \bar{a}_z$$

$$H = \frac{I a^2}{2(a^2+h^2)^{3/2}} \bar{a}_z$$

for N-Turns $\therefore H = \frac{N I a^2}{2(a^2+h^2)^{3/2}} \bar{a}_z$



if $h=0$ \Rightarrow

H عند مركز الحلقة

$$\therefore \bar{H} = \frac{I a^2}{2(a^2)^{3/2}} \bar{a}_z$$

$$\frac{I}{2a} \bar{a}_z$$

\rightarrow for N-Turns $\bar{H} = \frac{N I}{2a} \bar{a}_z$

Note:

المجال H عند مركز الحلقة θ

$$H = \frac{N I a^2}{2(a^2+h^2)^{3/2}} \rightarrow = \frac{N I a^2}{2 R^3} \times \frac{a}{a}$$

$$= \frac{N I}{2a} \left(\frac{a^3}{R^3} \right) \rightarrow \sin \theta = \frac{a}{R}$$

$$H = \frac{N I}{2a} \sin^3 \theta$$

$\rightarrow \theta \propto N I$

for any case To find $B \Rightarrow B = \mu H$ Tesla.

(7-2)

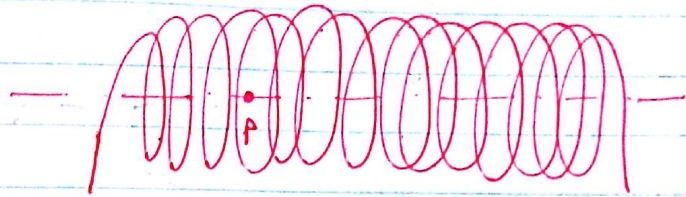
بند صیانه بعد از جلاش، سیم الی I و هوای سیم الی

$$J = \frac{NI}{L} \Rightarrow \text{منظری}$$

کثافت سیم الی طولی

I = سیم الی / طول سیم الی

$$J = \frac{I dz}{dz}$$



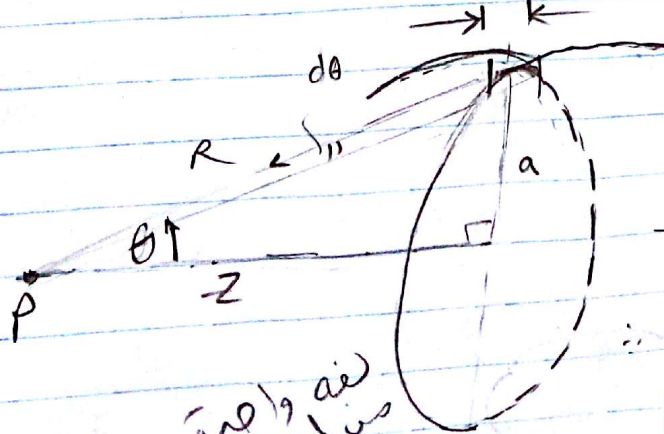
$$\frac{NI}{L} = \frac{I dz}{dz}$$

$$\int I dz = \frac{NI}{L} dz$$

$$dH_z = \frac{I dz}{2a} \sin^3 \theta$$

$$= \left(\frac{N}{L} \right) \frac{I}{2a} \sin^3 \theta dz$$

$$dH_z = \frac{n I}{2a} \sin^3 \theta dz$$



$$\sin \theta = \frac{a}{R}$$

$$\tan \theta = \frac{a}{z}$$

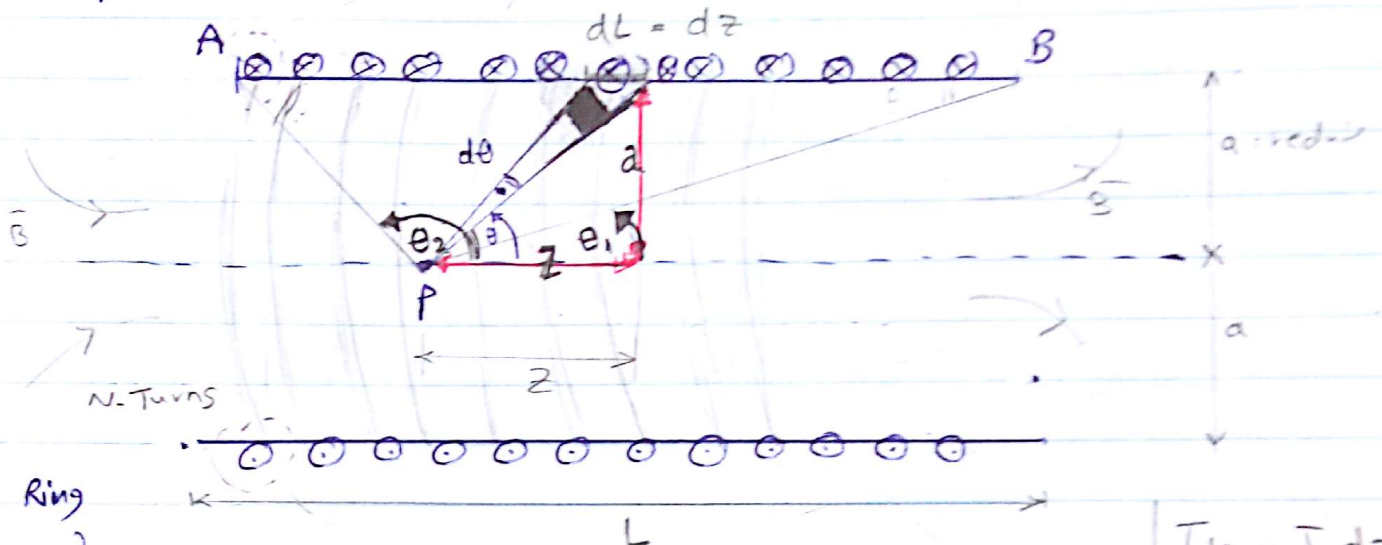
$$\cot \theta = \frac{z}{a}$$

$$z = a \cot \theta$$

بعد از جلاش
سیم الی الی
الی الی

(7-1) ✓

4
 [2] Required: \vec{H} on the axis of Solenoid



$$d\vec{H} = \frac{I dz}{2a} \sin \theta \hat{z}$$

$$\therefore dH_z = \frac{NI}{2a} \sin \theta^3 \left(\frac{dl}{L} \right), \quad dl = dz$$

$$= \left(\frac{N}{L} \right) \frac{I}{2a} \sin \theta^3 dz$$

$$= \left(\frac{n}{2a} \right) I \sin \theta^3 dz$$

$$\therefore dH_z = \frac{nI}{2a} \sin \theta^3 \times -\frac{1}{\sin^2 \theta} d\theta$$

$$= \frac{nI}{2} (-\sin \theta) d\theta$$

$$\therefore \vec{H}_z = \int_{\theta_1}^{\theta_2} dH_z$$

$$\vec{H}_z = -\frac{nI}{2} \int_{\theta_1}^{\theta_2} \sin \theta d\theta$$

$$I dz = J \cdot dz = \frac{I}{L} dz$$

من اشیاء Ring

ج. كثافة التيار الطولية J
 ج. كثافة التيار العرضي I
 $I dz = J \cdot dz$

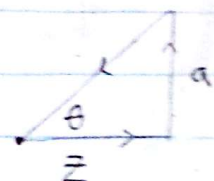
$$\tan \theta = \frac{a}{z}$$

$$\therefore \cot \theta = \frac{z}{a}$$

$$\therefore z = a \cot \theta$$

$$dz = -a \csc^2 \theta d\theta$$

$$\csc \theta = \frac{1}{\sin \theta}$$



$$H_z = \frac{n I}{2} [\cos \theta_1 - \cos \theta_2]$$

Note:

when P at terminal A $\Rightarrow \theta_2 = \pi/2$

$$H_z = \frac{n I}{2} \cos \theta_1$$

When P at terminal B $\Rightarrow \theta_1 = \pi/2$

$$H_z = \frac{n I}{2} \cos \theta_2$$

When \equiv in finit solenoid $\theta_1 = 0, \theta_2 = \pi$

$$H = n I$$

$$B = \mu_0 H$$

α_1 : الدائري بين العمودين الى الخط (Ray 1 & Ray 0)
 α_2 : الدائري بين العمودين الى الخط (Ray 2 & Ray 0)

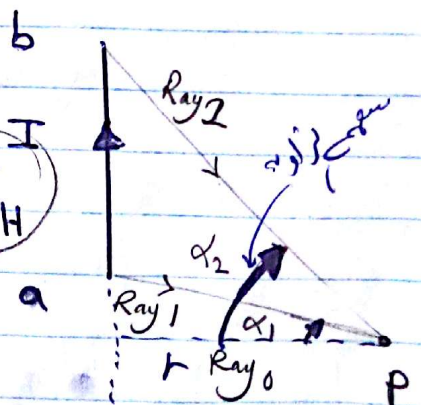
For finit line

$$\vec{a}_H = \vec{a}_I \times \vec{a}_r$$

$$H_p = \frac{I}{4\pi r} (\sin \alpha_2 - \sin \alpha_1) \vec{a}_H$$

البعد العمودي من النقطه الى الخط

من الاشياء



سهم الزاوية مع لتيار \oplus للزاوية \ominus للزاوية
 من العمود الى الخط

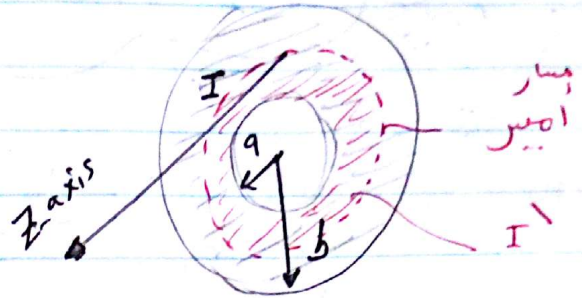
For infinit line: $\alpha_1 = -90$ $\alpha_2 = 90$

$$H_p = \frac{I}{2\pi r} \vec{a}_r$$

Ex 8] A hollow Conducting Cylinder, Find \vec{H} anywhere?
Solution

By using Ampere's law

$$\oint \vec{H} \cdot d\vec{\ell} = I_{enc}$$



For $r < a$ $\oint H \cdot d\ell = \text{Zero} \therefore \vec{H} = \text{Zero}$

$a < r < b$ $H_{\phi} \int_0^{2\pi} r d\phi = I' \Rightarrow$ جز من امپر، اگلی
 $H (2\pi r) = I \left(\frac{r^2 - a^2}{b^2 - a^2} \right)$ $J = \frac{I}{4\pi(b^2 - a^2)}$ کثافت امپر
 $\therefore \vec{H} = \frac{I}{2\pi r} \left(\frac{r^2 - a^2}{b^2 - a^2} \right) \vec{a}_{\phi}$ $\therefore I' = J 4\pi(r^2 - a^2)$
 $= \frac{I 4\pi(r^2 - a^2)}{4\pi(b^2 - a^2)}$

For $r > b$ $\oint H \cdot d\ell = I_{tot}$

$$H (2\pi r) = I$$

$$\vec{H}_{\phi} = \frac{I}{2\pi r} \vec{a}_{\phi}$$

$$\therefore \vec{H}_{\phi} = \begin{cases} \text{Zero} & r < a \\ \frac{I (r^2 - a^2)}{(b^2 - a^2)} & a < r < b \\ \frac{I}{2\pi r} & r > b \end{cases}$$

12

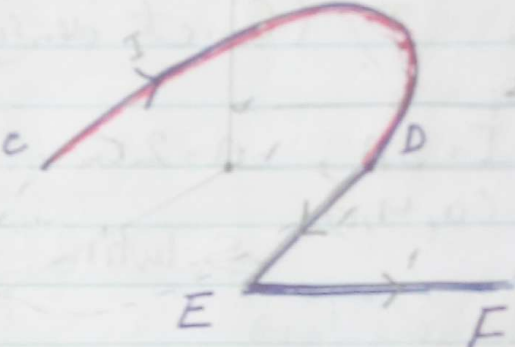
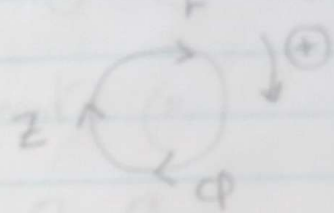
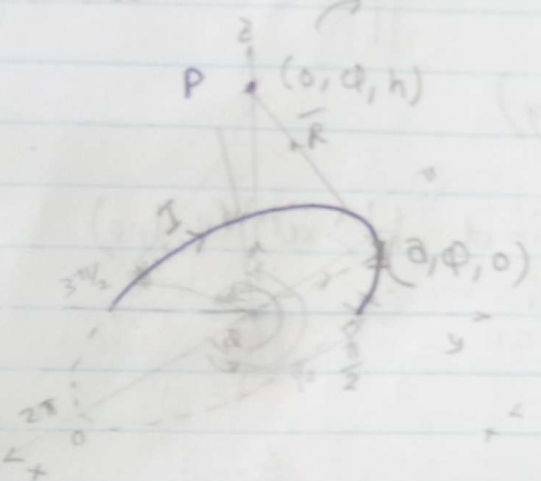
9 6

X X

5

3

رصف حلقه ← سلك كلى
الشكل لقياس ← تستخدم الجانوب
العام



$$R = \sqrt{a^2 + h^2}$$

$$d\vec{H} = \frac{I d\vec{l} \times \vec{R}}{4\pi R^3}$$

$$\vec{R} = -a \vec{a}_r + h \vec{a}_z$$

$$d\vec{l} = a d\phi \vec{a}_\phi$$

Point P
on the z-axis

$$d\vec{l} \times \vec{R} = (a d\phi \vec{a}_\phi) \times (-a \vec{a}_r + h \vec{a}_z)$$

$$= a^2 d\phi \vec{a}_z + ah d\phi \vec{a}_r$$

$$\phi = \pi/2$$

$$\therefore \vec{H} = \int d\vec{H} = \frac{I a^2}{4\pi R^3} \phi \Big|_{\frac{3\pi}{2}}^{\frac{\pi}{2}} \vec{a}_z$$

$$\phi = \frac{3\pi}{2}$$

$$+ \frac{I ah}{4\pi R^3} \phi \Big|_{\frac{3\pi}{2}}^{\frac{\pi}{2}} \vec{a}_r$$

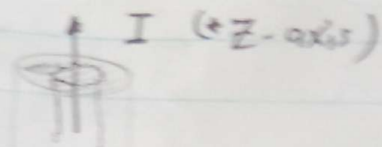
$$\vec{H} = - \frac{I a^2 \vec{a}_z + I ah \vec{a}_r}{4R^3}$$

* ستظهر مركبات \vec{a}_r و \vec{a}_z وذلك لعدم وجود
نماثل للحلقة حول نقطة الاصل (رصف حلقه فقط)

(2)

Ex [6]: Given: infinitely long Solid Conductor

a) Show that $H = \frac{I \rho}{2\pi a^2} \bar{a}_\rho$



b) Find J (Current density)

c) If $I = 3A$, $a = 2cm$. Find H at $(0, 1, 0)$ and $(0, 4, 0)$

Solution = 4

$\rho = \sqrt{0^2 + 4^2}$
 $\rho = 4$

a) Using Ampere's law

$$\oint H \cdot d\ell = I_{enc}$$

$$H \int_0^{2\pi} \rho d\phi = I'$$

$$H (2\pi\rho) = I \frac{\rho^2}{a^2}$$

$J = \frac{I}{4\pi a^2}$

$I' = J (4\pi\rho^2)$

$I' = I \frac{\rho^2}{a^2}$

$H (2\pi\rho) = I \frac{\rho^2}{a^2}$

$\therefore \bar{H} = \frac{I\rho}{2\pi a^2} \bar{a}_\rho$ #

b) $J = \nabla \times \bar{H} = -\frac{\partial H_\phi}{\partial z} \bar{a}_\phi + \frac{1}{\rho} \frac{\partial (\rho H_\phi)}{\partial \rho} \bar{a}_z$

$= \frac{I}{\rho} \cdot \frac{1}{2\pi a^2} \cdot 2\rho \bar{a}_z = \frac{I}{\pi a^2} \bar{a}_z$

c) at $(0, 1, 0) \Rightarrow$ inside the Conductor $\rho < a$

$\therefore H_\phi = \frac{I\rho}{2\pi a^2} = \frac{3 \times 1 \times 10^{-2}}{2\pi (4 \times 10^{-4})} = 11.94 \bar{a}_\phi \text{ A/m}$

at $(0, 4, 0) \Rightarrow$ outside $\Rightarrow \rho > a$

$\therefore H_\phi = \frac{I}{2\pi\rho} \bar{a}_\phi = \frac{3}{2\pi \times 4 \times 10^{-2}} = 11.94 \bar{a}_\phi \text{ A/m}$

12

10

at Center of the half ring

$$\rightarrow h = 0$$

$$\therefore \bar{H} = \frac{I a^2}{4 (a^2 + 0)^{3/2}} \bar{a}_2$$

$$\therefore \bar{H} = \frac{-I}{4a} \bar{a}_2$$

For part (CD) when $a \rightarrow 1$

$$\therefore \left[\bar{H}_P = \frac{-I}{4} \bar{a}_2 \right]$$

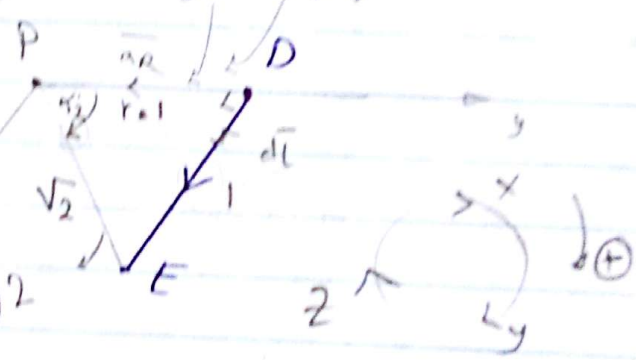
For part (DE)

Finite line $\rightarrow \bar{H}$ is finite

$$\alpha_1 = 0$$

$$\sin \alpha_2 = \frac{1}{\sqrt{2}}$$

Proj 2



$\alpha_2 (+ve) \rightarrow$ angle between \bar{a}_1 and \bar{a}_2

$$\begin{aligned} \bar{H}_P &\rightarrow \bar{a}_1 \times \bar{a}_2 \\ &= \bar{a}_x \times -\bar{a}_y \\ &= -\bar{a}_z \end{aligned}$$

$$\begin{aligned} \therefore H_P &= \frac{I}{4\pi r} (\sin \alpha_2 - \sin \alpha_1) (-\bar{a}_z) \\ &= \frac{I}{4\pi \times 1} \times \frac{1}{\sqrt{2}} (-\bar{a}_z) \end{aligned}$$

$$\left[\bar{H}_{P_2} = \frac{-I}{4\sqrt{2}\pi} \bar{a}_z \right]$$

Ex (7) given $\vec{H} = yz(x^2 + y^2)\vec{a}_x + y^2xz\vec{a}_y + 4x^2y^2\vec{a}_z$ A/m

- Determine \vec{J} at (5, 2, -3)
- \vec{I} passing through $x = -1$, $0 < y, z < 2$
- Show that $\nabla \cdot \vec{B} = \text{Zero}$.

Solution

$$a) \vec{J} = \nabla \times \vec{H} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ yz(x^2 + y^2) & -y^2xz & 4x^2y^2 \end{vmatrix}$$

$$\vec{J} = (8x^2y + xy^2)\vec{a}_x + [y(x^2 + y^2) - 4xy^2]\vec{a}_y + [-y^2z - z(x^2 + y^2)]\vec{a}_z$$

$$\text{at } (5, 2, -3) \Rightarrow \vec{J} = 420\vec{a}_x - 22\vec{a}_y + 99\vec{a}_z \text{ A/m}^2$$

$$b) I = \int \vec{J} \cdot d\vec{s}_x = \int_0^2 \int_0^2 (8x^2y + xy^2) dy dz$$

$$ds_x \leftarrow ds : \text{when } x = -1 \text{ to } y, z = 0 \text{ to } 2 \quad x = -1$$

$$\vec{J}_x \leftarrow \vec{J} \text{ at } x = -1 \quad = 53.33 \text{ A}$$

$$c) \vec{B} = \mu \vec{H}, \quad \nabla \cdot \vec{B} = 0 \rightarrow \nabla \cdot \vec{H} = 0$$

... لو اثبتنا انه ... $\nabla \cdot \vec{H} = 0$...

$$\therefore \nabla \cdot \vec{H} = \frac{\partial H_x}{\partial x} + \frac{\partial H_y}{\partial y} + \frac{\partial H_z}{\partial z}$$

$$= 2xyz - 2xyz = \text{Zero}$$

Hence, $\therefore \nabla \cdot \vec{B} = 0 \quad \#$

8 11

For EF

$\alpha_1, \alpha_2 (+ve)$

$$\sin \alpha_1 = \frac{1}{\sqrt{2}}$$

$$\sin \alpha_2 = \frac{2}{\sqrt{5}}$$

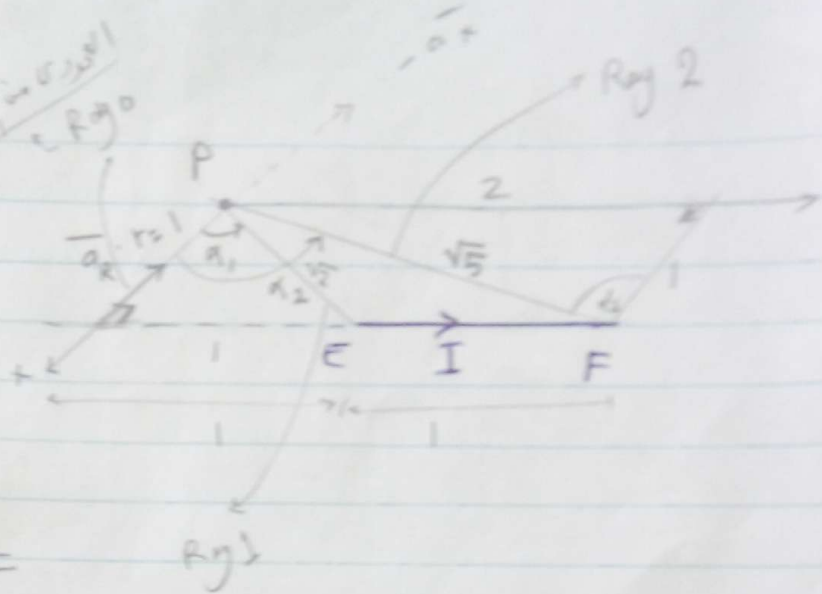
$$a_H = a_I \times a_R = \bar{a}_y \times -\bar{a}_x = \bar{a}_z$$

$$\therefore \bar{H}_{p_3} = \frac{I}{4\pi r} (\sin \alpha_2 - \sin \alpha_1) \bar{a}_H$$

$$\boxed{H_{p_3} = \frac{I}{4\pi \times 1} \left(\frac{2}{\sqrt{5}} - \frac{1}{\sqrt{2}} \right) \bar{a}_z}$$

$$\therefore \bar{H}_{\text{tot at } p} \Rightarrow \bar{H}_p = \bar{H}_{p_1} + \bar{H}_{p_2} + \bar{H}_{p_3}$$

$$\bar{H}_p = -\frac{I}{4} \bar{a}_z - \frac{I}{4\sqrt{2}\pi} \bar{a}_z + \frac{I}{4\pi} \left(\frac{2}{\sqrt{5}} - \frac{1}{\sqrt{2}} \right) \bar{a}_z$$



Force and Torque

Problem (1)

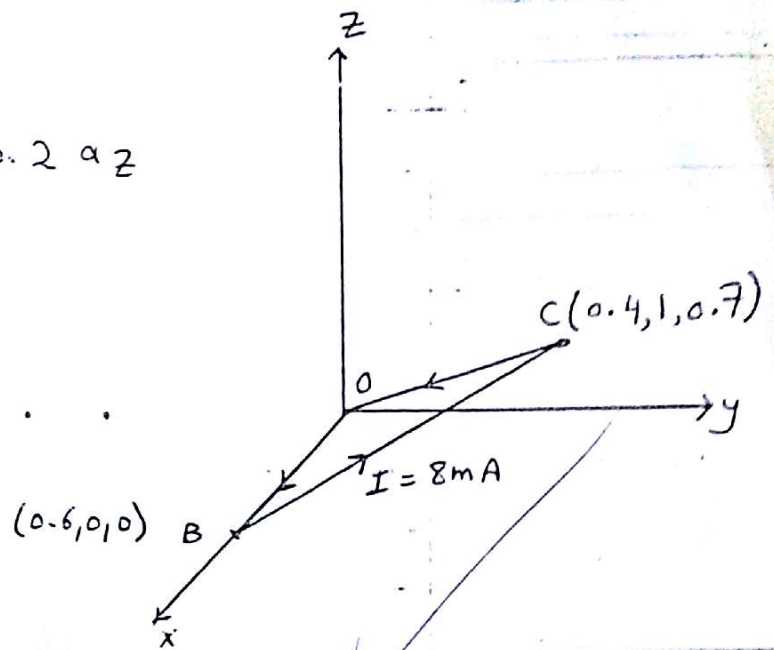
$$\vec{B} = 0.2 \vec{a}_x - 0.1 \vec{a}_y + 0.2 \vec{a}_z$$

find force on OBC

Solution

$$\vec{F} = \vec{F}_{OB} + \vec{F}_{BC} + \vec{F}_{CO}$$

$$\underline{\vec{F}_{OB}} \quad \vec{F}_{OB} = I \int d\vec{L} \times \vec{B}$$



$$d\vec{L} = dx \vec{a}_x$$

$$\therefore d\vec{L} \times \vec{B} = dx \vec{a}_x \times (0.2 \vec{a}_x - 0.1 \vec{a}_y + 0.2 \vec{a}_z)$$

$$= -0.1 dx \vec{a}_z + 0.2 dx (-\vec{a}_y)$$

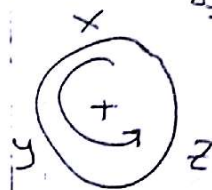
استخدم
المحدد أو
أي طريقة

$$= -0.1 dx \vec{a}_z - 0.2 dx \vec{a}_y$$

$$\vec{F}_{OB} = I \int_0^{0.6} (-0.1 dx \vec{a}_z - 0.2 dx \vec{a}_y)$$

$$= 8 \times 10^{-3} [-0.1 \times 0.6 \vec{a}_z - 0.2 \times 0.6 \vec{a}_y]$$

$$\vec{F}_{OB} = (-4.8 \vec{a}_z - 9.6 \vec{a}_y) \times 10^{-4} \text{ N.}$$



\vec{F}_{BC}

$$\vec{F}_{BC} = I \int d\vec{L} \times \vec{B}$$

$$d\vec{L} = dx \vec{a}_x + dy \vec{a}_y + dz \vec{a}_z$$

$$d\vec{L} \times \vec{B} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ dx & dy & dz \\ 0.2 & -0.1 & 0.2 \end{vmatrix} = (0.2 dy + 0.1 dz) \vec{a}_x - (0.2 dx - 0.2 dz) \vec{a}_y + (-0.1 dx - 0.2 dy) \vec{a}_z$$

$$\vec{F}_{BC} = I \int_{x=0.6}^{0.4} \int_{y=0}^1 \int_{z=0}^{0.7} \dots$$

Force and Torque

Problem ①

$$\vec{B} = 0.2 \vec{a}_x - 0.1 \vec{a}_y + 0.2 \vec{a}_z$$

find force on OBC

Solution

$$\vec{F} = \vec{F}_{OB} + \vec{F}_{BC} + \vec{F}_{CO}$$

$$\underline{\underline{\vec{F}_{OB}}} \quad \vec{F}_{OB} = I \int d\vec{L} \times \vec{B}$$

$$d\vec{L} = dx \vec{a}_x$$

$$\therefore d\vec{L} \times \vec{B} = dx \vec{a}_x \times (0.2 \vec{a}_x - 0.1 \vec{a}_y + 0.2 \vec{a}_z)$$

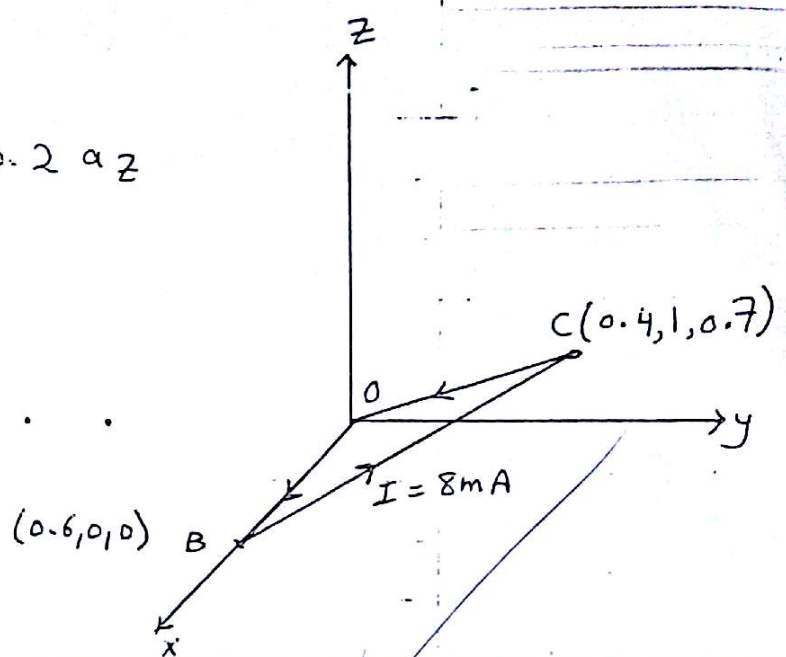
$$= -0.1 dx \vec{a}_z + 0.2 dx (-\vec{a}_y)$$

$$= -0.1 dx \vec{a}_z - 0.2 dx \vec{a}_y$$

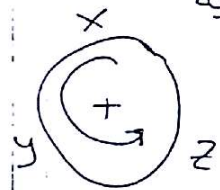
$$\vec{F}_{OB} = I \int_0^{0.6} (-0.1 dx \vec{a}_z - 0.2 dx \vec{a}_y)$$

$$= 8 \times 10^{-3} [-0.1 \times 0.6 \vec{a}_z - 0.2 \times 0.6 \vec{a}_y]$$

$$\vec{F}_{OB} = (-4.8 \vec{a}_z - 9.6 \vec{a}_y) \times 10^{-4} \text{ N}$$



استخدم
المحدد أو
أي طريقة



$$\underline{\underline{\vec{F}_{BC}}} \quad \vec{F}_{BC} = I \int d\vec{L} \times \vec{B}$$

$$d\vec{L} = dx \vec{a}_x + dy \vec{a}_y + dz \vec{a}_z$$

$$d\vec{L} \times \vec{B} = \begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ dx & dy & dz \\ 0.2 & -0.1 & 0.2 \end{vmatrix} = (0.2dy + 0.1dz) \vec{a}_x - (0.2dx - 0.2dz) \vec{a}_y + (-0.1dx - 0.2dy) \vec{a}_z$$

$$\vec{F}_{BC} = I \int_{x=0.6}^{0.4} \int_{y=0}^{0.7} \int_{z=0}^{0.7} \dots$$

$$F_{BC} = 8 \times 10^{-3} \left[(0.2 \times 1 + 0.1 \times 0.7) a_x - (0.2 \times (0.4 - 0.6) - 0.2 \times 0.7) a_y + (-0.1 \times (0.4 - 0.6) - 0.2 \times 1) a_z \right]$$

$$= (2.16 a_x + 1.44 a_y - 1.44 a_z) \times 10^{-3} \text{ N}$$

$\underline{F_{CO}}$ $dL = dx a_x + dy a_y + dz a_z$ مركبات متجهية
لـ dL

$dL \times B \rightarrow$ مركبات متجهية
لـ $dL \times B$

$$F_{CO} = 8 \times 10^{-3} \int_{x=0.4}^0 \int_{y=1}^0 \int_{z=0.7}^0 \dots$$

$$= 8 \times 10^{-3} \left[(0.2 \times -1 + 0.1 \times -0.7) a_x - (0.2 \times -0.4 - 0.2 \times -0.7) a_y + (-0.1 \times -0.4 - 0.2 \times -1) a_z \right]$$

$$F_{CO} = (-2.16 a_x - 0.48 a_y + 1.92 a_z) \times 10^{-3} \text{ N}$$

$$F_t = F_{OB} + F_{BC} + F_{CO} \text{ N}$$

$$F_t = \text{Zero N} \quad \#$$

Problem (2)

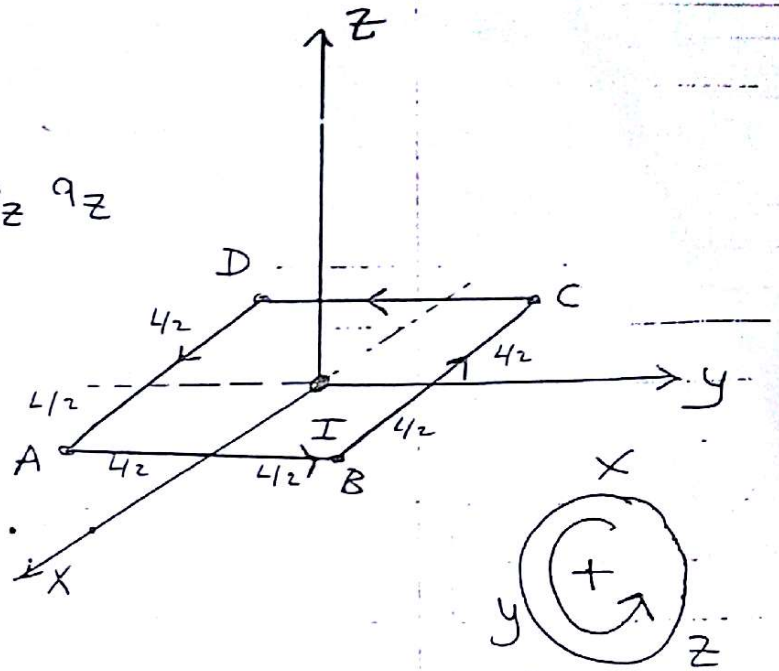
$$\mathbf{B} = B_x \mathbf{a}_x - B_y \mathbf{a}_y + B_z \mathbf{a}_z$$

Find F

Solution

$$\mathbf{F} = I \int d\mathbf{L} \times \mathbf{B}$$

وهنا 4 أجزاء



(AB)

$$d\mathbf{L} = dy \mathbf{a}_y$$

$$d\mathbf{L} \times \mathbf{B} = dy \mathbf{a}_y \times (B_x \mathbf{a}_x - B_y \mathbf{a}_y + B_z \mathbf{a}_z)$$

$$= B_x dy (-\mathbf{a}_z) + B_z dy (\mathbf{a}_x)$$

$$d\mathbf{L} \times \mathbf{B} = dy (-B_x \mathbf{a}_z + B_z \mathbf{a}_x)$$

أو استخدم
المحددات

$$\begin{aligned} \mathbf{F}_{AB} &= I \int_{y=-L/2}^{L/2} d\mathbf{L} \times \mathbf{B} = I [-B_x \mathbf{a}_z + B_z \mathbf{a}_x] L \\ &= LI (-B_x \mathbf{a}_z + B_z \mathbf{a}_x) \end{aligned}$$

(BC)

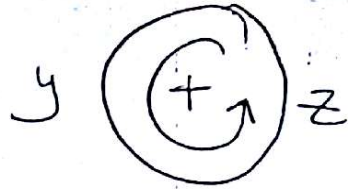
$$d\mathbf{L} = dx \mathbf{a}_x$$

$$d\mathbf{L} \times \mathbf{B} = dx \mathbf{a}_x \times (B_x \mathbf{a}_x - B_y \mathbf{a}_y + B_z \mathbf{a}_z)$$

$$= dx (-B_y \mathbf{a}_z + B_z (-\mathbf{a}_y))$$

$$\begin{aligned} \mathbf{F}_{BC} &= I \int_{x=+L/2}^{-L/2} d\mathbf{L} \times \mathbf{B} = -LI [-B_y \mathbf{a}_z - B_z \mathbf{a}_y] \\ &= LI [B_y \mathbf{a}_z + B_z \mathbf{a}_y] \end{aligned}$$

(CD) $dL = dy \, a_y$



$$dL \times \vec{B} = dy \, a_y \times (B_x a_x - B_y a_y + B_z a_z)$$

$$= dy (-B_x a_z + B_z a_x)$$

$$F_{CD} = I \int_{y=-L/2}^{+L/2} dL \times B = -IL (-B_x a_z + B_z a_x)$$

$$= IL (B_x a_z - B_z a_x)$$

DA $dL = dx \, a_x$

$$dL \times B = dx \, a_x \times (B_x a_x - B_y a_y + B_z a_z)$$

$$= dx (-B_y a_z + B_z (-a_y))$$

$$F_{DA} = I \int_{x=-L/2}^{+L/2} dL \times B = IL [-B_y a_z - B_z a_y]$$

$$\therefore F_t = F_{AB} + F_{BC} + F_{CD} + F_{DA} = \text{Zero} \quad \#$$

Conclusion:-

In uniform field \rightarrow Force on closed path

$$F = I \oint dL \times B = -I B \times \oint dL$$

$$= \text{Zero}$$

$$\oint dL = \text{Zero}$$

القوة المؤثرة على مسار مغلق في مجال منتظم تساوي صفر

③ Force between two parallel lines.

Currents in Opposite directions

field on ① due to ②

$$H_{21} = \frac{I}{2\pi d} a_\phi$$

$$a_\phi = a_{z_1} \times a_{z_2} = -a_z \times (-a_y) = -a_x$$

الدالة المتجهة

$$H_{21} = \frac{I}{2\pi d} (-a_x)$$

$$B_{21} = \frac{\mu_0 I}{2\pi d} (-a_x)$$

Force on ① $F_1 = I \int d\vec{L}_1 \times \vec{B}_{21}$

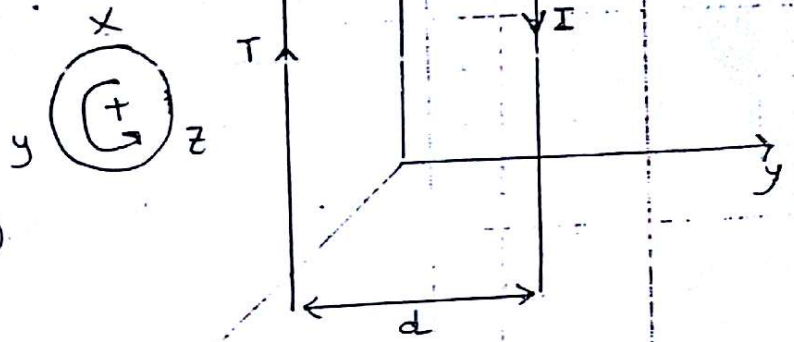
$$F_1 = I \int_0^{\text{length}} \frac{-\mu_0 I}{2\pi d} dz a_y$$

$$F_1 = -\frac{\mu_0 I^2}{2\pi d} (\text{length}) a_y$$

$$\frac{F_1}{\text{length}} = \frac{\mu_0 I^2}{2\pi d} (-a_y) \rightarrow \text{Repulsive force} \quad \text{قوة مسافة}$$

$$|F_2| = |F_1| \quad \text{دفع الأجزاء العكس}$$

(ay)



$$dL_1 = dz a_z$$

$$dL_1 \times B_{21} = dz a_z \times \left(\frac{\mu_0 I}{2\pi d} \right) (-a_x)$$

$$= -\frac{\mu_0 I}{2\pi d} dz (a_z \times a_x)$$

$$= -\frac{\mu_0 I}{2\pi d} dz (a_y)$$

B is on \hat{a}_z direction

[5] $\vec{B} = B \hat{a}_z$

Find Force

$$F = I \int d\vec{L} \times \vec{B}$$

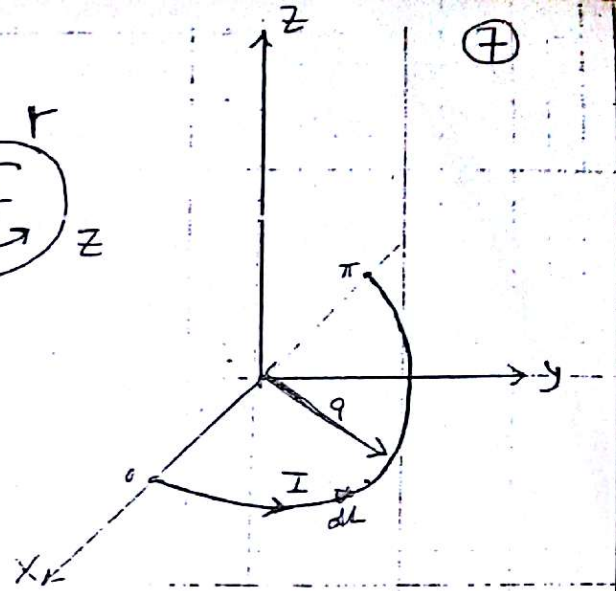
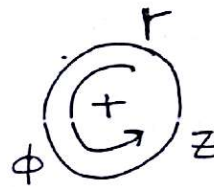
$$d\vec{L} = a d\phi \hat{a}_\phi \quad \vec{B} = B \hat{a}_z$$

$$d\vec{L} \times \vec{B} = a B d\phi (\hat{a}_\phi \times \hat{a}_z)$$

$$= a B d\phi \hat{a}_r$$

$$F = I \int_{\phi=0}^{\pi} a B d\phi \hat{a}_r$$

$$F = \pi a B I \hat{a}_r \quad \#$$



6

$$\vec{B} = 0.5 \hat{a}_z$$

المقاومة 50Ω على $6V$

Solution

$$I = \frac{V}{R} = \frac{6}{50} = 0.12 A$$

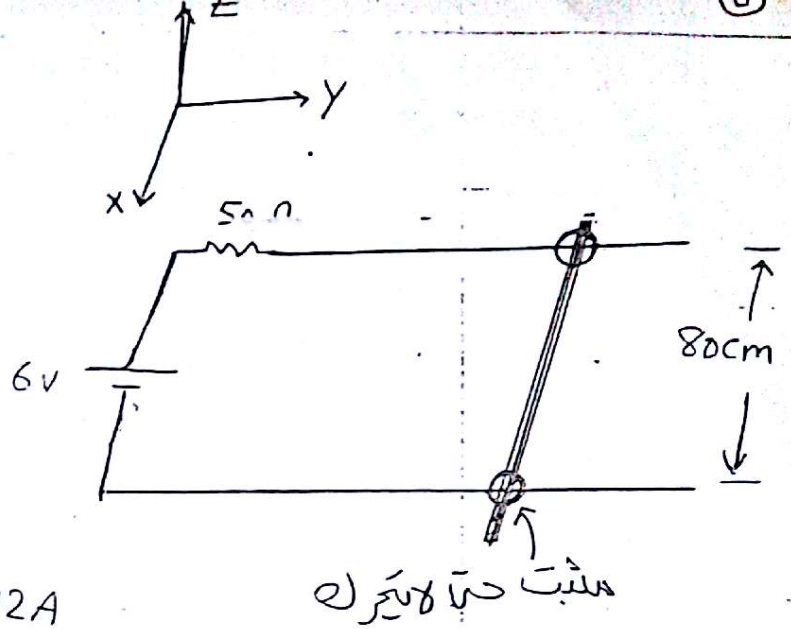
$$\vec{L} = 0.8 \hat{a}_x$$

$$\vec{F} = I \vec{L} \times \vec{B} = (0.12 * 0.8 * 0.5) (\hat{a}_x \times \hat{a}_z)$$

$$\vec{F} = 0.048 (-\hat{a}_y)$$

$$|F| = 0.048 \text{ N}$$

$$\text{direction } \vec{a}_F = -\hat{a}_y \quad \#$$



As a numerical example of these equations, consider Fig. 9.2. We have a square loop of wire in the $z = 0$ plane carrying 2 mA in the field of an infinite filament on the y axis, as shown. (We desire the total force on the loop.)

Solution. The field produced in the plane of the loop by the straight filament is

$$H = \frac{I}{2\pi x} a_z = \frac{15}{2\pi x} a_z \quad \text{A/m}$$

Therefore,

$$B = \mu_0 H = 4\pi \times 10^{-7} H = \frac{3 \times 10^{-6}}{x} a_z \quad \text{T}$$

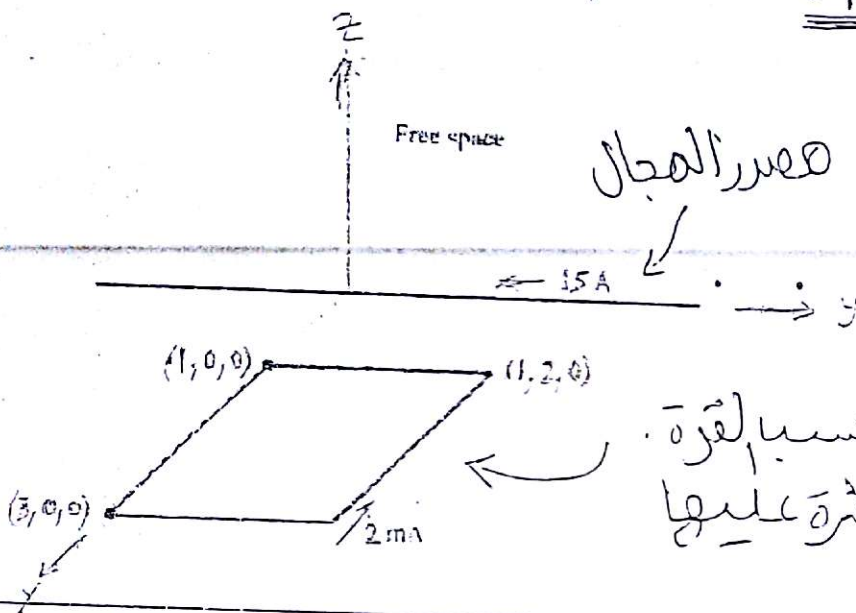
We use the integral form (10),

$$F = -I \oint B \times dL$$

$$\text{or } \underline{\underline{F}} = I \int d\mathbf{L} \times \mathbf{B}$$

نقطة الحل

مصدر المجال



احسب القوة
المؤثرة عليها

Let us assume a rigid loop so that the total force is the sum of the forces on the four sides. Beginning with the left side:

$$\begin{aligned} F &= -2 \times 10^{-3} \times 3 \times 10^{-6} \left[\int_{x=1}^3 \frac{a_z}{x} \times dx a_x + \int_{y=0}^2 \frac{a_z}{3} \times dy a_y \right. \\ &\quad \left. + \int_{x=3}^1 \frac{a_z}{x} \times dx a_x + \int_{y=2}^0 \frac{a_z}{1} \times dy a_y \right] \\ &= -6 \times 10^{-9} \left[\ln x \Big|_1^3 a_y + \frac{1}{3} y \Big|_0^2 (-a_x) + \ln x \Big|_3^1 a_y + y \Big|_2^0 (-a_x) \right] \\ &= -6 \times 10^{-9} \left[(\ln 3) a_y - \frac{2}{3} a_x + \left(\ln \frac{1}{3} \right) a_y + 2 a_x \right] \\ &= -8 a_y \quad \mu\text{N} \end{aligned}$$

أوجدتها
كل ضلع
لو حده فمادة
للتسهيل
على نفسك

Thus, the net force on the loop is in the $-a_y$ direction.

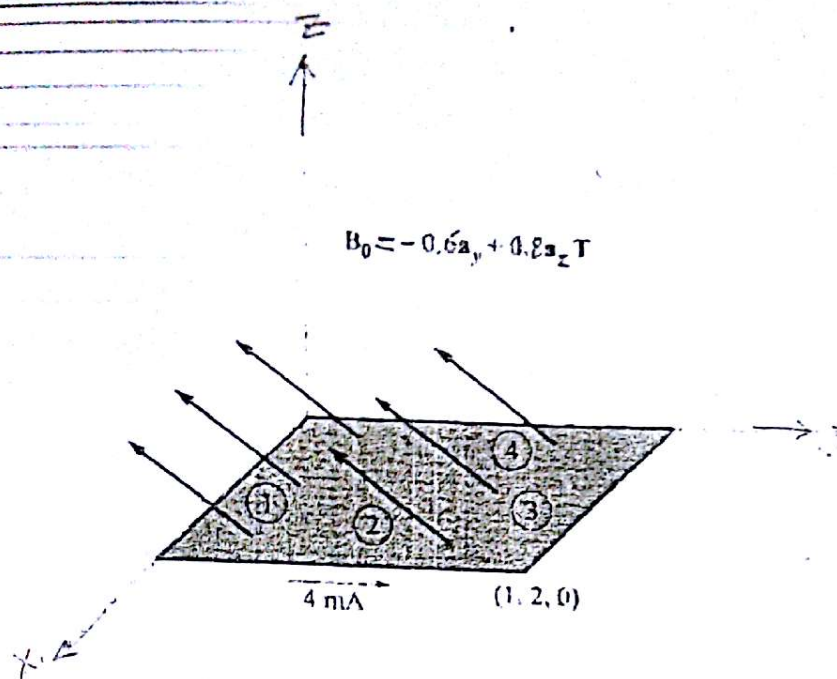


FIGURE 9.7

A rectangular loop is located in a uniform magnetic flux density B_0 .

Example 9.3

To illustrate some force and torque calculations, consider the rectangular loop shown in Fig. 9.7. Calculate the torque by using $\mathbf{T} = \mathbf{r} \times \mathbf{F}$.

Solution. The loop has dimensions of 1 m by 2 m and lies in the uniform field $B_0 = -0.6\mathbf{a}_x + 0.8\mathbf{a}_z \text{ T}$. The loop current is 4 mA, a value that is sufficiently small to avoid causing any magnetic field that might affect B_0 .

We have

$$\mathbf{T} = 4 \times 10^{-3} [(1)(2)\mathbf{a}_z] \times (-0.6\mathbf{a}_x + 0.8\mathbf{a}_z) = 4.8\mathbf{a}_y \text{ mN} \cdot \text{m}$$

Thus, the loop tends to rotate about an axis parallel to the positive x -axis. The small magnetic field produced by the 4-mA loop current tends to line up with B_0 .

Example 9.4

Now let us find the torque once more, this time by calculating the total force and torque contribution for each side.

Solution. On side 1 we have

$$\begin{aligned} \mathbf{F}_1 &= I\mathbf{L}_1 \times \mathbf{B}_0 = 4 \times 10^{-3} (1\mathbf{a}_x) \times (-0.6\mathbf{a}_x + 0.8\mathbf{a}_z) \\ &= -3.2\mathbf{a}_y + 2.4\mathbf{a}_z \text{ mN} \end{aligned}$$

On side 3 we obtain the negative of this result.

$$\mathbf{F}_3 = 3.2\mathbf{a}_y + 2.4\mathbf{a}_z \text{ mN}$$

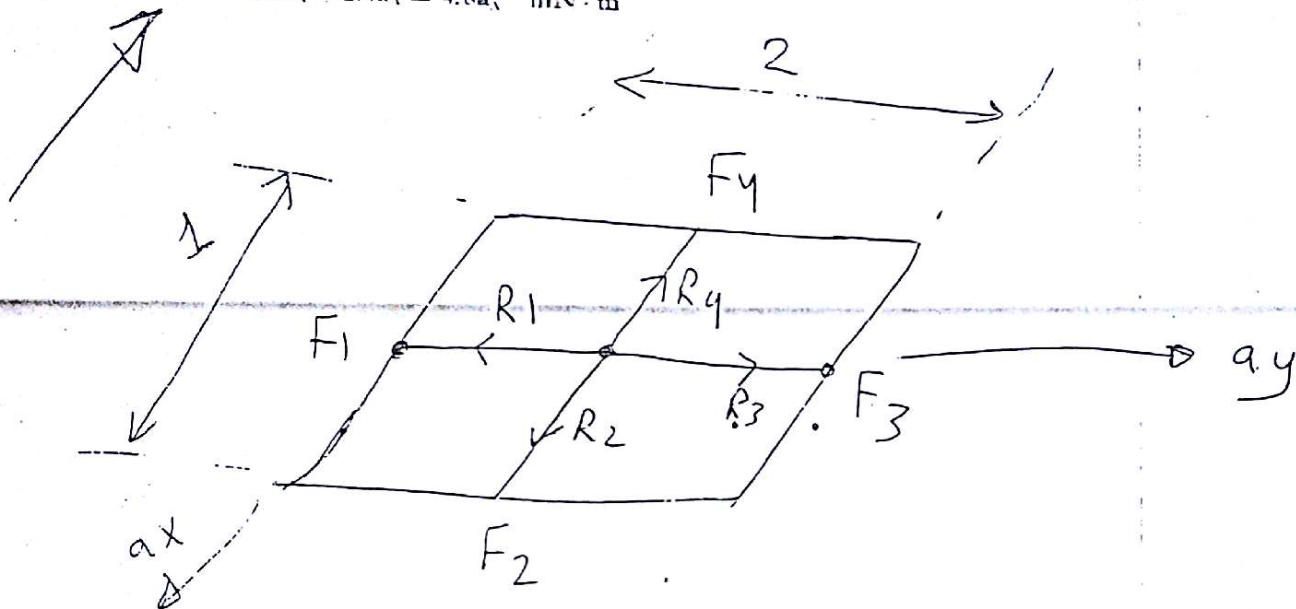
$$F_2 = I L_2 \times B_0 = 4 \times 10^{-3} (2a_1) \times (-0.6a_1 + 0.8a_2) \\ = -6.4a_1 \text{ mN}$$

with side 4 again providing the negative of this result.

$$F_4 = -6.4a_1 \text{ mN}$$

Since these forces are distributed uniformly along each of the sides, we treat each force as if it were applied at the center of the side. The origin for the torque may be established anywhere since the sum of the forces is zero, and we choose the center of the loop. Thus,

$$T = T_1 + T_2 + T_3 + T_4 = R_1 \times F_1 + R_2 \times F_2 + R_3 \times F_3 + R_4 \times F_4 \\ = (-1a_1) \times (-3.2a_2 - 2.4a_2) + (0.5a_1) \times (6.4a_1) \\ + (1a_1) \times (3.2a_2 + 2.4a_2) + (-0.5a_1) \times (-6.4a_1) \\ = 2.4a_1 + 2.4a_1 = 4.8a_1 \text{ mN} \cdot \text{m}$$

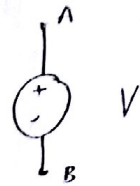


$$\begin{cases} R_1 = -1a_y \\ R_3 = 1a_y \end{cases} \quad \begin{cases} R_2 = 0.5a_x \\ R_4 = -0.5a_x \end{cases}$$

* Magnetic Circuit

In electric field:

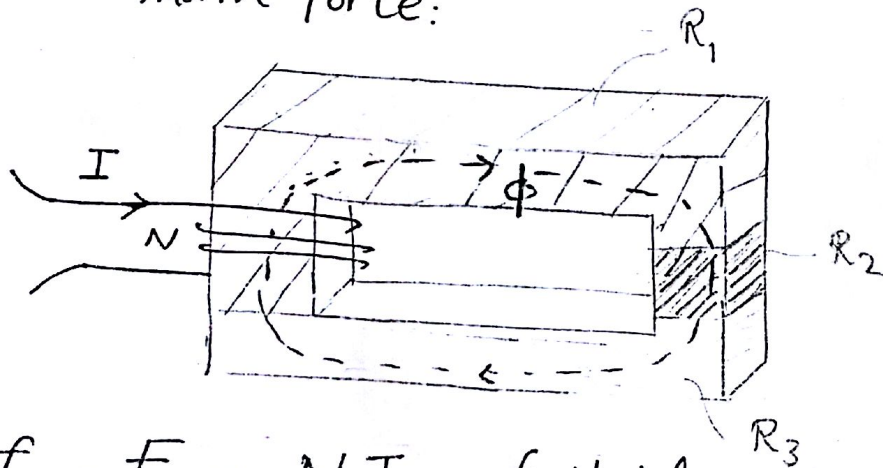
$$V_{AB} = - \int_A^B \mathbf{E} \cdot d\mathbf{l}$$



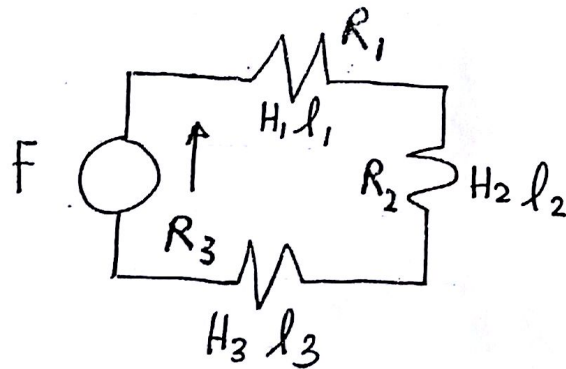
For magnetic field

$$\text{mmf} = V_{\text{mmf}} = F = \int_A^B \mathbf{H} \cdot d\mathbf{l}$$

↳ Magnetic motive force:



$$\text{mmf} = F = NI = \oint \mathbf{H} \cdot d\mathbf{l}$$



$$F = \int_1 \mathbf{H}_1 \cdot d\mathbf{l} + \int_2 \mathbf{H}_2 \cdot d\mathbf{l} + \int_3 \mathbf{H}_3 \cdot d\mathbf{l}$$

$$= H_1 L_1 + H_2 L_2 + H_3 L_3$$

$$NI = \sum HL$$

Magnetic Torque and Moment

$$\vec{m} = I \vec{S} \vec{a}_n \quad \text{A/m}^2$$

magnetic dipole moment

$$\vec{T} = \vec{m} \times \vec{B}$$

Magnetization in materials

$$\vec{B} = \mu_0 (\vec{H} + \vec{M})$$

$$\vec{M} = \chi_m \vec{H}$$

magnetic susceptibility of the medium

$$\vec{J}_b = \nabla \times \vec{M}, \quad K_b = \vec{M} \times \vec{a}_n$$

classification of magnetic materials

- Diamagnetic $\mu_r < 1.0$
- Para " $\mu_r \approx 1$
- Ferro " $\mu_r \gg 1$

K_b : bound surface current density
 J_b : " volume "

Ex 8.7
 Pg. 336

Magnetic Boundary Conditions

$$\oint \vec{B} \cdot d\vec{s} = \mu_0 I_{enc}, \quad \oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$\vec{B}_{in} = \vec{B}_{out}$$

$$\mu_1 H_{in} = \mu_2 H_{out}$$

$$H_{1t} = H_{2t}$$

$$(\vec{H}_1 - \vec{H}_2) \cdot \vec{a}_{n12} = K$$

free current density

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_1}{\mu_2}$$

unit vector normal to the interface and directed from ① → ②
 for free of current media or not conductors

Ex 8.8) Pg. 338

(and Ex 8.9) Pg. 340

$$\therefore K = 0$$

Magnetic Torque and Moment

$$\vec{m} = I \vec{S} \vec{a}_n \quad \text{A/m}^2$$

magnetic dipole moment

$$\vec{T} = \vec{m} \times \vec{B}$$

Magnetization in materials

$$\vec{B} = \mu_0 (\vec{H} + \vec{M})$$

$$\vec{M} = \chi_m \vec{H}$$

magnetic susceptibility of the medium

$$\vec{J}_b = \nabla \times \vec{M}, \quad K_b = \vec{M} \times \vec{a}_n$$

classification of magnetic materials

- Diamagnetic $\mu_r < 1.0$
- Para " $\mu_r \approx 1$
- Ferro " $\mu_r \gg 1$

K_b : bound surface current density
 J_b : " volume "

Ex (8.7)
Pg. 336

Magnetic Boundary Conditions

$$\oint \vec{B} \cdot d\vec{s} = I_{enc}, \quad \oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$B_{1n} = B_{2n}$$

$$\Rightarrow \mu_1 H_{1n} = \mu_2 H_{2n}$$

$$H_{1t} = H_{2t}$$

$$(H_1 - H_2) a_{n12} = K \quad \text{free current density}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\mu_1}{\mu_2}$$

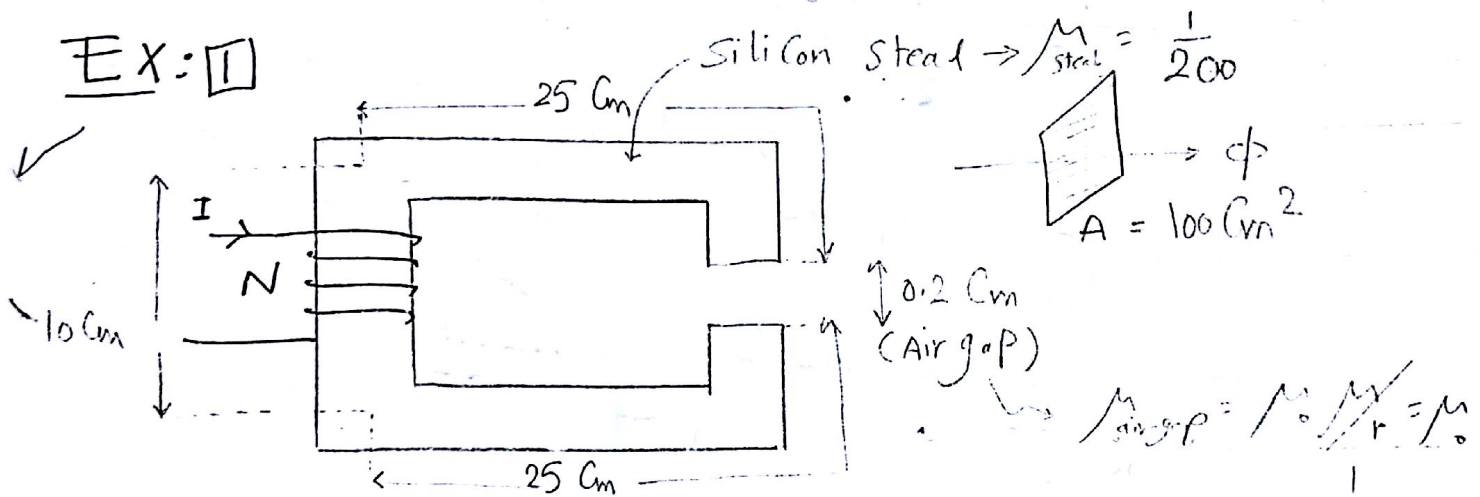
unit vector normal to the interface and directed from ① → ②
 for free of current media or not conductors

$$\therefore K = 0$$

Ex 8.8) Pg. 338

(and Ex 8.9) Pg. 340

$\therefore H = \frac{B}{\mu}, B = \frac{\phi}{A}$ طول مسلك الفيض
 $\therefore NI = \sum \phi \frac{L}{\mu A}$ كثرة قوا الفيض
 $\therefore NI = \sum \phi R$ magnetic Reluctance
 المقاومة الحثائية
 $NI = \phi (R_1 + R_2 + R_3)$



Find N ? $\Rightarrow B = 1 \text{ Tesla}, I = 10 \text{ A}$
 Solution

$\text{mmf}_{\text{tot}} = NI = \text{mmf}_{\text{steel}} + \text{mmf}_{\text{air}}$

① $\text{mmf}_{\text{air}} = \phi R_{\text{air}}$

$\phi = B \times A_g = 1 \times 25 \times 10^{-4} = 25 \times 10^{-4} \text{ wb}$
 $R_{\text{air}} = \frac{l_g}{\mu_0 \mu_r A_g} = \frac{0.2 \times 10^{-2}}{\mu_0 \times 25 \times 10^{-4}}$
 $\mu_0 = 4\pi \times 10^{-7}$

$= 636 \times 10^3 \text{ AT/wb}$

$\therefore \text{mmf}_{\text{air}} = 25 \times 10^{-4} + 636.6 \times 10^3 = 1590 \text{ AT}$

EX 8.7 Pg. 336

given: Region $0 \leq z \leq 2$ is occupied by material ($\mu_r = 2.5$). if $B = 10y \bar{a}_x - 5x \bar{a}_y \frac{\text{mwb}}{\text{m}^2}$
determine: J, J_b, M, K_b on $z=0$

Solution

a) $J = \nabla \times H = \nabla \times \frac{B}{\mu_0 \mu_r}$

$$\begin{aligned} &= \frac{1}{\mu_0 (2.5)} \left[\frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y} \right] \bar{a}_z \\ &= \frac{10^6}{\pi} (-5 - 10) \times 10^{-3} \bar{a}_z \\ J &= -4.775 \bar{a}_z \text{ KA/m}^2 \end{aligned}$$

b) J_b (bound volume current density)
 $= \chi_m J = (\mu_r - 1) J$
 $= (2.5 - 1) \times -4.775 \times 10^{-3}$
 $J_b = -7.163 \text{ KA/m}^2$

c) $M = \chi_m H = \chi_m \frac{B}{\mu_0 \mu_r} = (\mu_r - 1) \left(\frac{B}{\mu_0 \mu_r} \right)$
(magnetization)
 $= \frac{1.5 \times [10y \bar{a}_x - 5x \bar{a}_y]}{\mu_0 (2.5)} = \frac{4.775 \times \bar{a}_x}{-2.387 \times \bar{a}_y} \frac{\text{KA}}{\text{m}}$

d) K_b (bound surface current density)

$$\begin{aligned} K_b &= M \times \bar{a}_n \quad \because z=0 \therefore \bar{a}_n = -\bar{a}_z \\ &= (4.775 \bar{a}_x - 2.387 \bar{a}_y) \times (-\bar{a}_z) \\ K_b &= 2.387 \bar{a}_x + 4.775 \bar{a}_y \text{ KA/m} \end{aligned}$$

$$(2) \text{ mmf}_{\text{Steel}} = \text{mmf}_{25\text{cm}} + \text{mmf}_{25\text{cm}} + \text{mmf}_{10\text{cm}}$$

$$= 2 * \phi R_{25\text{cm}} + \phi * R_{10\text{cm}}$$

$$R_{25\text{cm}} = \frac{l_{25\text{cm}}}{\mu_{\text{steel}} A_s} = \frac{25 \times 10^{-2}}{\frac{1}{200} * 25 \times 10^{-4}} = \underline{2000 \text{ AT/wb}}$$

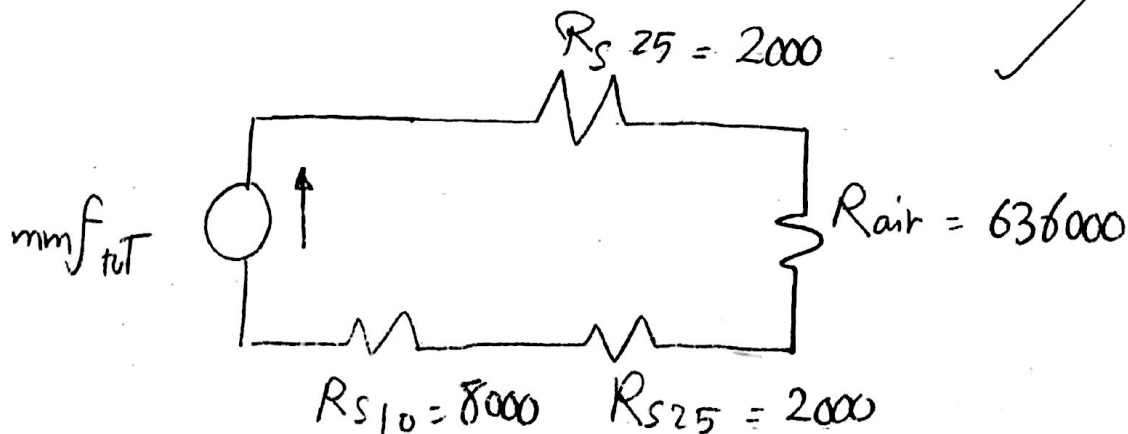
$$R_{10\text{cm}} = \frac{l_{10\text{cm}}}{\mu_{\text{steel}} A_s} = \frac{10 \times 10^{-2}}{\frac{1}{200} * 25 \times 10^{-4}} = \underline{8000 \text{ AT/wb}}$$

$$\therefore \text{mmf}_{\text{Steel}} = 2 * 25 \times 10^{-4} (2000) + 25 \times 10^{-4} * 8000 = 30 \text{ AT}$$

$$\therefore \text{mmf}_{\text{tot}} = 1590 + 30 = 1620 \text{ Tesla}$$

$$= NI = N * 10$$

$$\therefore N = \frac{1620}{10} = 162 \text{ Turn}$$



Given: $\vec{H} = -2\vec{a}_x + 6\vec{a}_y + 4\vec{a}_z$ A/m
in region $y - x - 2 \leq 0$ where

$\mu_1 = 5\mu_0$ Calc:

a) M_1 & B_1

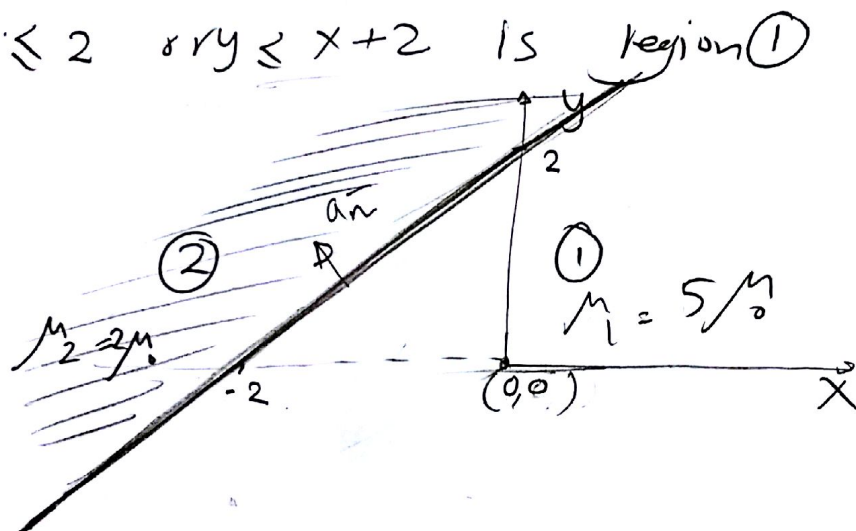
b) H_2 & B_2 in region $y - x - 2 > 0$
where $\mu_2 = 2\mu_0$

Since

Solution

$\therefore y - x - 2 = 0$ is the Plane

$\therefore y - x \leq 2$ or $y \leq x + 2$ is region ①



magnetization

a) $M_1 = \chi_{m1} H_1$

$= (\mu_{r1} - 1) H_1 = (5 - 1) (-2, 6, 4)$

$= -8\vec{a}_x + 24\vec{a}_y + 16\vec{a}_z$ A/m

flux density

$B_1 = \mu_1 H_1 = \mu_0 \mu_{r1} H_1 = \mu_0 (5) (-2, 6, 4)$

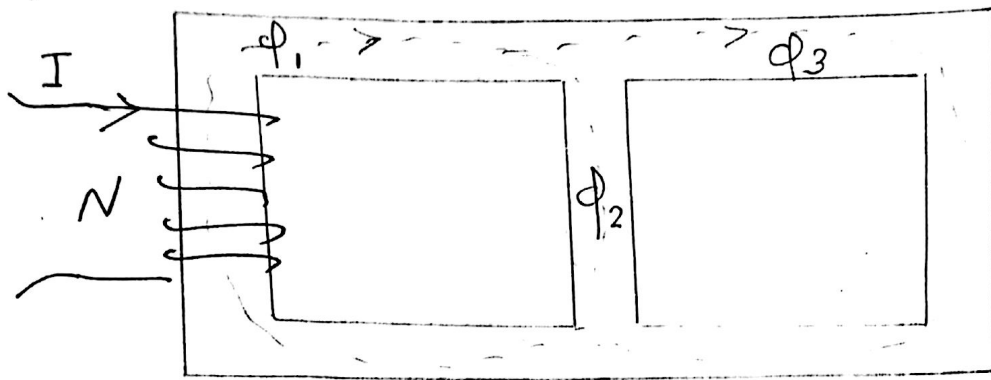
$= -12.57\vec{a}_x + 37.7\vec{a}_y + 25.13\vec{a}_z$ $\mu Wb/m^2$

b) $H_{1n} = (H_1 \cdot a_n) a_n$

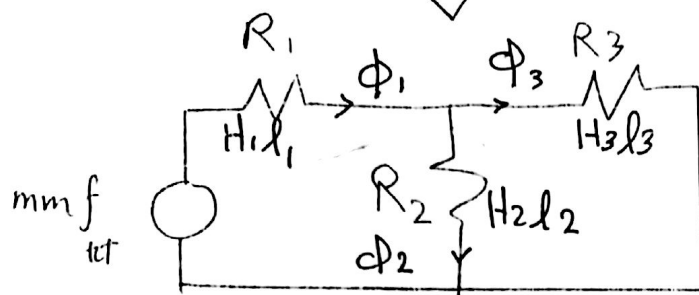
$= [(-2, 6, 4) \cdot \left(\frac{-1, 1, 0}{\sqrt{2}}\right)] \left(\frac{-1, 1, 0}{\sqrt{2}}\right)$

$\vec{H}_{1n} = -4\vec{a}_x + 4\vec{a}_y$

✓ For Parallel Magnetic Circuit:



نفس قواعد الدوائر الكهربائية



$$\Phi_1 = \Phi_2 + \Phi_3$$

$$NI - H_1 l_1 = H_2 l_2 = H_3 l_3$$

$$\therefore NI = \Phi_1 \left(R_1 + \frac{R_2 \times R_3}{R_2 + R_3} \right) \leftarrow \begin{matrix} NI - \Phi_1 R_1 = \Phi_2 R_2 \\ = \Phi_3 R_3 \end{matrix}$$

Stored energy in magnetic circuit:-

$$W_m = \frac{1}{2} \int_{V_0} B \cdot H \, dv = \frac{1}{2} LI^2$$

$$= \frac{1}{2} \int_{V_0} \mu H^2 \, dv = \frac{1}{2\mu} \int_{V_0} B^2 \, dv$$

✓ Self Inductance : $L = \frac{\lambda}{I}$ Flux linkage
الفيض المترابطة

$$= \frac{N\Phi}{I} = N \int B \cdot ds$$

التيار : I الفيض : Φ

$$H_1 = H_{1n} + H_{1t}$$

$$\therefore H_{1t} = H_1 - H_{1n} = (-2, 8, 4) - (-4, 4, 0) \\ = 2\bar{a}_x + 2\bar{a}_y + 4\bar{a}_z$$

Using Boundary Conditions

$$\therefore H_{2t} = H_{1t} = 2\bar{a}_x + 2\bar{a}_y + 4\bar{a}_z$$

$$B_{2n} = B_{1n}$$

$$\therefore \mu_2 H_{2n} = \mu_1 H_{1n}$$

$$\therefore H_{2n} = \frac{\mu_1}{\mu_2} (H_{1n}) = \frac{5}{2} (-4\bar{a}_x + 4\bar{a}_y)$$

$$H_{2n} = -10\bar{a}_x + 10\bar{a}_y$$

$$\therefore H_2 = H_{2t} + H_{2n} \\ = -8\bar{a}_x + 12\bar{a}_y + 4\bar{a}_z \text{ A/m}$$

$$\therefore B_2 = \mu_2 H_2 = \mu_2 \mu_0 H_2 \\ = -20.11\bar{a}_x + 30.16\bar{a}_y \\ + 10.05\bar{a}_z \text{ mT/m}^2$$

called. self Inductance

✓ EX: [2] Find the inductance of a coaxial cable per unit length.

Solution
Using Ampere law

$$I_{enc} = \oint H \cdot dl$$

- For $a < r < b$

$$\oint H \cdot dl = I$$
$$H (2\pi r) = I$$

$$\therefore H = \frac{I}{2\pi r}$$

$$\lambda = \frac{1}{\mu_0} \oint B \cdot d\mathbf{s} = \mu_0 \int_a^b H \cdot d\mathbf{s}$$

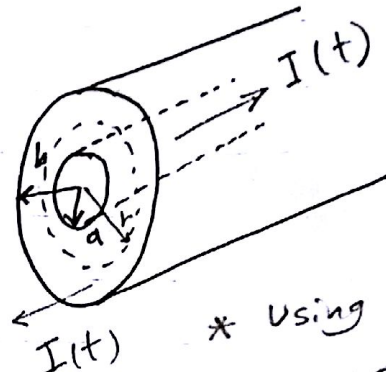
$$= \mu_0 \frac{I}{2\pi} \int_a^b \int_0^{2\pi} \frac{1}{r} dr d\phi$$

$$= \frac{\mu_0 I}{2\pi} \left[\phi \right]_0^{2\pi} \left[\ln r \right]_a^b$$

$$= \frac{\mu_0 I}{2\pi} \ln \frac{b}{a}$$

$$L = \frac{\lambda}{I} = \frac{\mu_0}{2\pi} \ln \frac{b}{a} \quad \text{H/m}$$

Ampere law $\leftarrow H \leftarrow B \leftarrow \phi \leftarrow \lambda ?$



* using cylindrical coordinates (r, ϕ, z)

Notes: $\frac{B}{H}$ B H curve - Permeability Curve

X EX (3) given:
Uniform Cross section Area
 $= 2 \text{ cm}^2$

$$N = 500$$

$$\phi = 0.2 \text{ mwb}$$

$$\mu_{\text{air gap}} = 0.00333 = \frac{1}{300}$$

$$\mu_{\text{cast}} = 0.001 = \frac{1}{1000}$$

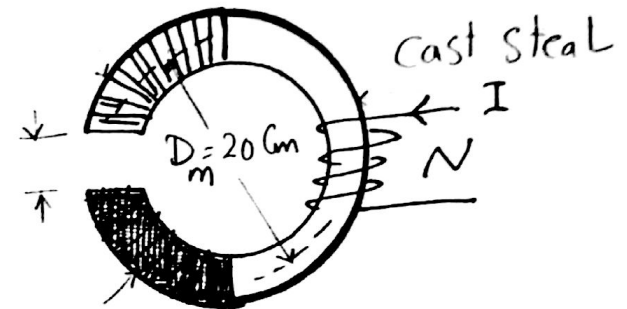
$$\mu_{\text{silicon}} = \frac{1}{2300}$$

Find I ?

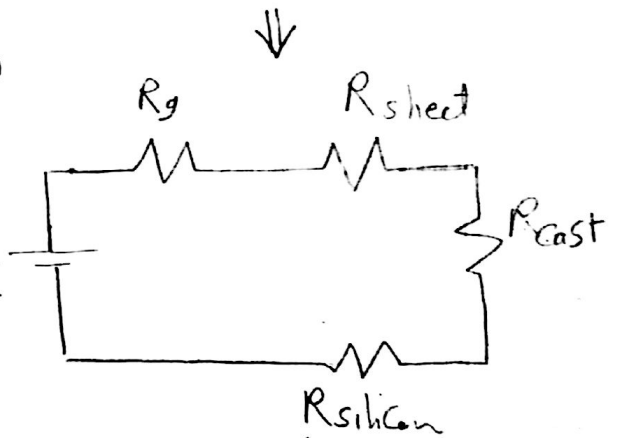
$$B = \phi / A$$

$$= \frac{0.2 \times 10^{-3}}{2 \times 10^{-4}} = 1 \text{ Tesla}$$

Sheet steel



silicon steel



$$R_g = \frac{l_g}{\mu_0 A} = \frac{0.05}{\mu_0 \times 2 \times 10^{-4}} = 198.94 \times 10^6$$

$$R_{\text{sheet}} = \frac{l_{\text{sh}}}{\mu_{\text{sh}} A}$$

الطول المسار في الحديد

$$l_{\text{sh}} = \frac{\pi D_m}{4} = \frac{\pi}{20} \text{ m}$$

$$= \frac{\pi/20}{\frac{1}{300} \times 2 \times 10^{-4}} = 235.62 \times 10^3 \text{ AT/wb}$$

$$R_{\text{cast}} = \frac{l_{\text{cast}}}{\mu_{\text{cast}} A}$$

الطول المسار في الحديد

$$l_{\text{cast}} = \frac{\pi D_m}{2} = \frac{\pi}{10}$$

$$= \frac{\pi/10}{\frac{1}{1000} \times 2 \times 10^{-4}} = 1.57 \times 10^6 \text{ AT/wb}$$

$$R_{\text{silicon}} = \frac{l_{\text{silic}}}{\mu_{\text{silic}} \times A} \quad , \quad l_{\text{silicon}} = \frac{\pi D_m}{4} = \frac{\pi}{20} \text{ m}$$

$$= \frac{\pi/20}{\frac{1}{2300} \times 2 \times 10^{-4}} = 1.806 \times 10^6 \text{ AT/wb}$$

$$\therefore R_{\text{tot}} = R_{\text{cast}} + R_{\text{sheet}} + R_{\text{sheet}} + R_g$$

$$= 202.55 \times 10^6 \text{ AT/wb}$$

$$NI = \phi R_{\text{tot}}$$

$$500 I = 0.2 \times 10^{-3} \times 202.55 \times 10^6$$

$$\therefore I = 81.022 \text{ A}$$

$$L = \frac{NI}{\phi} = \frac{500 \times 81.022}{0.2 \times 10^{-3}} \text{ H}$$

$$= R$$

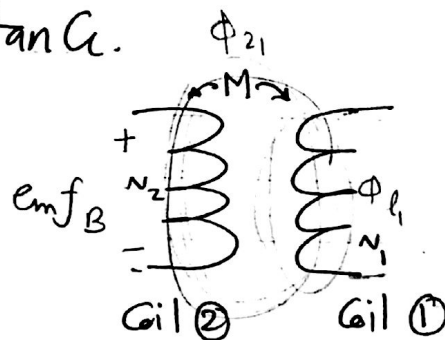
* Mutual Inductance.

$$M_{21} = \frac{\lambda_{21}}{I_1}$$

$$= \frac{N_2 \phi_{21}}{I_1}$$

Similarly

$$M_{12} = \frac{N_1 \phi_{12}}{I_2}$$



لفيض الناتج من الملف
① و يمر به الملف
② و يقطع الملف

For linear magnetic Circuit:

$$M_{12} = M_{21} = M$$

Ex ④: Two Coils A & B

✓ $\phi_{BA} = 60\% \phi_A$, $I_A = 6A$, $\phi_A = 1.08 \text{ mwb}$
 $N_B = 1500 \text{ Turns}$

Find a) Mutual induct
b) $E_B = \text{emf induced in Coil B}$
 when I_A is reduced to zero
 in $1 \text{ ms} = \frac{\Delta I_A}{\Delta t} = \left(\frac{6}{1 \times 10^{-3}} \right)$

Solution

$$M_{BA} = \frac{N_B \phi_{BA}}{I_A} = \frac{1500 \times 1.08 \times 10^{-3}}{6} = 0.27 \text{ H}$$

$$\text{emf}_B = M \frac{dI_A}{dt} = M \frac{\Delta I_A}{\Delta t} = 0.27 \times \frac{6}{1 \times 10^{-3}} = 1620 \text{ Volt}$$

* القوة الدافعة الكهربية المستحثة ← تنشأ عندما يكون هناك معدل
 تغير في الفيض (أو التيار)
 بالسيارة للزمن
 على الملف (B) نتيجة وجود
 فيض متغير من مصدر الملف (A)

$$\therefore \frac{dI}{dt} \Rightarrow \frac{d\phi}{dt} \xrightarrow{\text{تنشأ}} \text{emf}$$

Force and Torque in magnetic Field

$$\vec{F} = Q \vec{u} \times \vec{B}$$

\vec{u} السرعة في خط المجال المغناطيسي
 \vec{B} المجال المغناطيسي

if there's additional Electric field \vec{E}

$$\therefore \vec{F}_{\text{Tot}} = Q (\vec{E} + \vec{u} \times \vec{B})$$

Ex: given: $\vec{B} = 5 \text{ mT } (-\hat{a}_z)$

$\vec{u} = 83.5 \text{ Km/s } (\hat{a}_x)$

$Q = 1.6 \times 10^{-9} \text{ C}$

what electric Field (E) present if

$F_{\text{net}} = \text{Zero}$
Solution

$$\vec{F}_{\text{mag}} = Q \vec{u} \times \vec{B}$$

$$= Q u (\hat{a}_x) \times B (-\hat{a}_z)$$

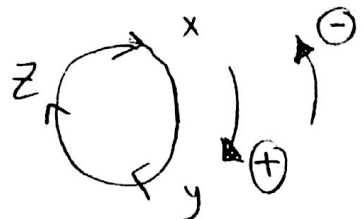
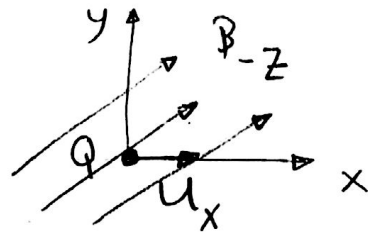
$$\vec{F}_{\text{mag}} = Q u B \hat{a}_y$$

for $F_{\text{net}} = 0$

$$\therefore F_{\text{elect}} = |F_{\text{mag}}| - \hat{a}_y$$

$$\therefore Q E = Q u B$$

$$= (83.5 \times 10^3) \times (5 \times 10^{-3}) \text{ V/m}$$



Magnetic Force on a differential Current element

$$d\vec{F} = dQ (\vec{u} \times \vec{B}) \quad , \quad I = \frac{dQ}{dt} \quad , \quad \frac{d\vec{u}}{dt} = d\vec{l}$$

$$d\vec{F} = I (d\vec{l} \times \vec{B})$$

$$\therefore \vec{F} = I (\vec{L} \times \vec{B}) \rightarrow \text{motor theory.}$$

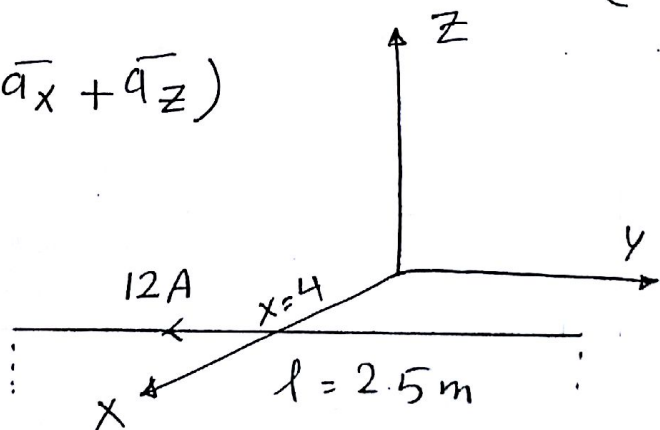
ایک خاص صورت میں

Ex[2]: Given: A Conductor length $L = 2.5 \text{ m}$
at $z=0$, $x=4 \text{ m}$, $I = 1.2 \text{ A}$ in $(-\hat{a}_y)$

$$\vec{F} = \frac{1.2 \times 10^{-2}}{\sqrt{2}} (-\hat{a}_x + \hat{a}_z)$$

Find \vec{B} ?

$$\vec{F} = I (\vec{L} \times \vec{B})$$



$$I (\vec{L} \times \vec{B}) = 12 \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0 & -2.5 & 0 \\ B_x & B_y & B_z \end{vmatrix} = (-30 B_z) \hat{a}_x + (30 B_x) \hat{a}_z$$

$$\therefore B_z = B_x = \frac{4 \times 10^{-4}}{\sqrt{2}} \text{ T} \quad = \frac{1.2 \times 10^{-2}}{\sqrt{2}} (-\hat{a}_x + \hat{a}_z)$$

$B_y \rightarrow$ have any value.

Work and Power

$$W = \int_{\text{int}}^{\text{fin}} \vec{F}_a \cdot d\vec{l}$$

terminal
or K
→ applied work

F_a : applied force
Field force from magnetic
opposite to force

$$P = \frac{dW}{dt} = \frac{\vec{F}_a \cdot d\vec{l}}{dt}, \quad \vec{F}_a = -I \vec{L} \times \vec{B}$$

$$P = \vec{F}_a \cdot \vec{u}$$

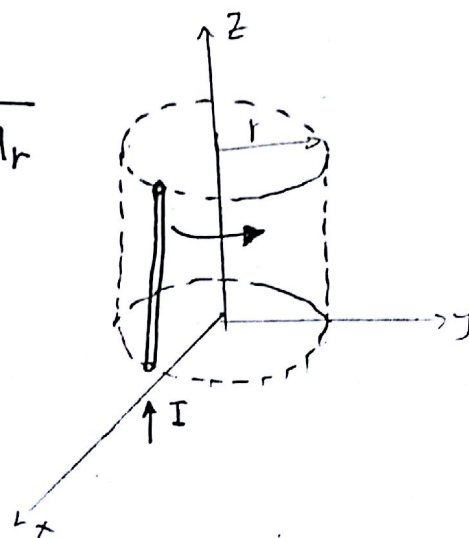
Ex (3) given: $\vec{B} = B_0 \vec{a}_r$

Find F, W, P ?

$$\vec{F}_{\text{mag}} = I \vec{L} \times \vec{B}$$

$$= I L (\vec{a}_z) \times B_0 (\vec{a}_r)$$

$$= I L B_0 \vec{a}_\phi$$



$$\vec{F}_a = -B_0 I L (\vec{a}_\phi) = B_0 I L (-\vec{a}_\phi)$$

$$W = \int_{\text{int}}^{\text{fin}} \vec{F}_a \cdot d\vec{l}, \quad d\vec{l} = r d\phi \vec{a}_\phi$$

$$= - \int_0^{2\pi} B_0 I L r d\phi = -2\pi B_0 I L$$

full revolution

$$P = \frac{W}{t} = \frac{2\pi B_0 I L}{(60/\pi)}$$

$$\text{Torque: } \vec{T} = \vec{r} \times \vec{F}$$

$$= r (\vec{a}_r) \times B_0 I L (-\vec{a}_\phi)$$